CELL	DESCRIPTION	GROUP
D00001	Name Plate	GP & E
D00003	Temporary Concrete Barrier	GP & E
D00004	Total Bill of Material, 15 line	GP & E
D00005	Total Bill of Material, 20 line	GP & E
D00006	Total Bill of Material, 25 line	GP & E
D00007	Total Bill of Material, 30 line	GP & E
D00010	Section thru integral abutment for PPC beams	GP & E
D00011	Section thru integral abutment for steel beams	GP & E
D00012	Section thru pile supported stub abutment for PPC beams	GP & E
D00013	Section thru pile supported stub abutment for steel beams	GP & E
D00014	Section thru semi-integral abutment for PPC beams	GP & E
D00015	Section thru semi-integral abutment for steel beams	GP & E
D00016	Riprap for section thru abutments (use with D00010 through D00015)	GP & E
D00017	Slopewall for section thru abutments (use with D00010 through D00015)	GP & E
D00018	Section Thru Filled Vaulted Abutment	GP & E
D00020	Parapet Joint Details	Superstructure
D00021	Parapet Joint at Sidewalk	Superstructure
D00022	Section thru sidewalk	Superstructure
D00023	42" Section thru parapet for base sheet S-D or S-I-D	Superstructure
D00024	d(E) bar bending diagram for 42" parapet for base sheet S-D or S-I-D	Superstructure
D00025	42" parapet joint details for base sheet S-D or S-I-D	Superstructure
D00026	Anchor rod for light pole mounted on parapet	Superstructure
D00027	d2(E) bar bending diagram for parapet with light pole	Superstructure
D00028	d3(E) bar bending diagram for parapet with light pole	Superstructure
D00029	Plan view of parapet with light pole, conduit inside parapet	Superstructure
D00030	Section A-A of parapet with light pole, conduit inside parapet	Superstructure
D00031	Plan view of parapet with light pole	Superstructure
D00032	Section A-A of parapet with light pole, conduit outside parapet	Superstructure
D00033	Inside Elevation of 42" Parapet for superstructure detail sheet	Superstructure
D00040	Drainage Scupper, DS-11 details	Drainage
D00041	Drainage Scupper, DS-11 details	Drainage
D00042	Drainage Scupper, DS-12 details	Drainage
D00043	Drainage Scupper, DS-12 details	Drainage

CELL	DESCRIPTION	GROUP				
D00044	Drainage Scupper, DS-12M10 details	Drainage				
D00045	Drainage Scupper, DS-33 details	Drainage				
D00046	4 in x 12 in drain details	Drainage				
D00050	Strip seal joint for deck beams with CWS	Joint				
Note: Cells [	Note: Cells D00060 thru D00069 are to be used as required on PPC Deck Beam Superstructure sheets where sections are to be inserted.					
D00060	Sect thru fixed abut for 11" PPC deck beam with conc. wearing surface and approach slab	Deck Beams				
D00061	Sect thru fixed abut. for 11" PPC deck beam with HMA wearing surface and approach slab	Deck Beams				
D00062	Sect thru fixed abut. for 17" and 21" PPC deck beams with conc. wearing surface and approach slab	Deck Beams				
D00063	Sect thru fixed abut. for 17" and 21" PPC deck beams with HMA wearing surface and approach slab	Deck Beams				
D00064	Sect thru fixed abut. for 27", 33", and 42" PPC deck beams with conc. wearing surface and approach slab	Deck Beams				
D00065	Sect thru fixed abut. for 27", 33", and 42" PPC deck beams with HMA wearing surface and approach slab	Deck Beams				
D00066	Sect thru fixed abut. for 11" thru 42" PPC deck beams with conc. wearing surface without approach slab	Deck Beams				
D00067	Sect thru fixed abut. for 11" thru 42" PPC deck beams with HMA wearing surface without approach slab	Deck Beams				
D00068	Sect thru fixed pier for 11" thru 42" PPC deck beams with concrete wearing surface	Deck Beams				
D00069	Sect thru fixed pier for 11" thru 42" PPC deck beams with HMA wearing surface	Deck Beams				
D00070	Plan View of alternate fixed bearings at abutments	Deck Beams				
D00071	Plan View of alternate fixed bearings at pier	Deck Beams				
D00072	Sect thru fixed abut. with alternate fixed bearings	Deck Beams				
D00073	Sect thru fixed pier with alternate fixed bearings	Deck Beams				
D00074	Sect thru expansion abut. for 11" PPC deck beams with conc. wearing surface	Deck Beams				
D00075	Sect thru expansion abut. for 17" and 21" PPC deck beams with conc. wearing surface and approach slab	Deck Beams				
D00076	Sect thru expansion abut. for 17" and 21" PPC deck beams with HMA wearing surface and approach slab	Deck Beams				
D00077	Sect thru expansion abut. for 27", 33", and 42" PPC deck beams with conc. wearing surface and approach slab	Deck Beams				
D00078	Sect thru expansion abut. for 27", 33", and 42" PPC deck beams with HMA wearing surface and approach slab	Deck Beams				
D00079	Sect thru expansion abut. for 11" thru 42" PPC deck beams with conc. wearing surface without approach slab	Deck Beams				
D00080	Sect thru expansion abut. for 17" thru 42" PPC deck beams with HMA wearing surface without approach slab	Deck Beams				
D00081	Sect thru expansion pier for 11" thru 42" PPC deck beams with conc. wearing surface	Deck Beams				
D00082	Sect thru expansion pier for 17" thru 42" PPC deck beams with HMA wearing surface	Deck Beams				
D00083	Retainer angle at expansion joint of deck beams	Deck Beams				
D00084	Shear key clamping details at stage construction joint	Deck Beams				
D00090	Bearing detail for integral abutment with steel beams	Bearing				
D00100	Stud shear connector details	Structural Steel				
D00101	Interior diaphragm beam or girder up to 42"	Structural Steel				

CELL	DESCRIPTION	GROUP
D00102	Interior diaphragm plate girder < 48"	Structural Steel
D00103	End diaphragm for wide flange beams	Structural Steel
D00104	End diaphragm for shallow plate girders	Structural Steel
D00105	End diaphragm for plate girders < 48" and skew < 45 deg with finger plate or modular joints	Structural Steel
D00110	End diaphragm stage construction sequence for wide flange beams	Structural Steel
D00111	End diaphragm stage construction sequence for plate girders	Structural Steel
D00120	Wide flange splice detail (outside flange plates only)	Structural Steel
D00130	LRFD data tables (Non-composite in negative moment regions)	Design Tables
D00131	LRFD data tables (Composite in negative moment regions)	Design Tables
D00132	LRFD data tables for curved girders	Design Tables
D00133	LRFD PPC I beam data tables	Design Tables
D00134	LFD data tables	Design Tables
D00135	LFD data tables for curved girders	Design Tables
D00136	LFD PPC I beam data tables	Design Tables
D00140	Geotextile wall form brace details	Wall
D00141	Geotextile wall procedure	Wall
D00155	Permanent bracing details for IL27 & IL36 beams	Superstructure
D00156	Permanent bracing details for IL45 & IL54 beams	Superstructure
D00157	Permanent bracing details for IL63 & IL72 beams	Superstructure
D00158	Permanent bracing detail - No skew	Superstructure
D00159	Permanent bracing detail - Skewed	Superstructure
D00160	Permanent bracing details for 36" & 42" PPC I beams	Superstructure
D00161	Permanent bracing details for 48" & 54" PPC I beams	Superstructure
D00162	Permanent bracing details for Bulb T beams	Superstructure
D00163	Bar splicer assembly for edge beams at stage construction joint	Superstructure
D00170	View E-E for Bridge approach slabs with 42" parapets	Approach Slabs
D00200	Dead load deflection diagram for top of slab elevations	TOS Elevations
D00201	PPC Bulb T-beam fillet height detail for top of slab elevations	TOS Elevations
D00202	PPC I-beam fillet height detail for top of slab elevations	TOS Elevations

Cell Name: D00001 Descrip: Name Plate

STATION

BUILT BY

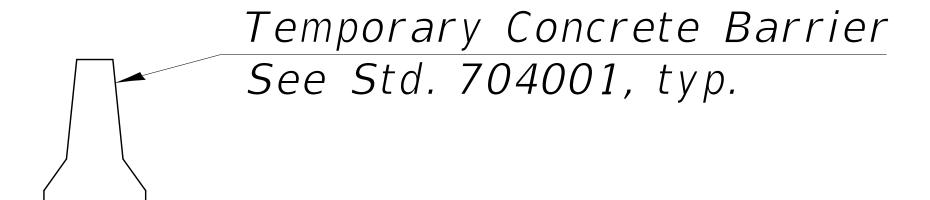
STATE OF ILLINOIS

LOADING HL-93

STRUCTURE NO.

NAME PLATE
See Std. 515001

Descrip: Temporary Concrete Barrier



Descrip: Total Bill of Material, 15 line

# TOTAL BILL OF MATERIAL

ITEM	UNIT	SUPER	SUB	TOTAL

Descrip: Total Bill of Material, 20 line

# TOTAL BILL OF MATERIAL

ITEM	UNIT	SUPER	SUB	TOTAL

Descrip: Total Bill of Material, 25 line

TOTAL BILL OF MATERIAL

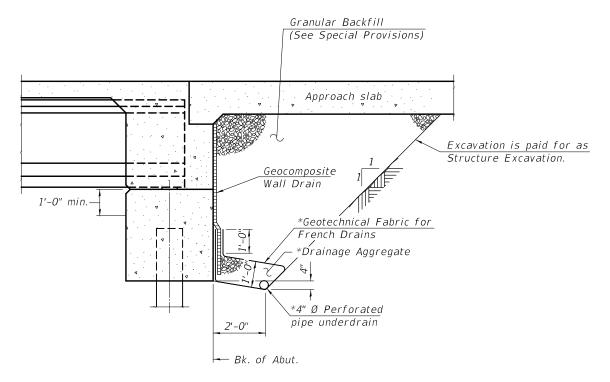
ITEM	UNIT	SUPER	SUB	TOTAL
				_

Descrip: Total Bill of Material, 30 line

TOTAL BILL OF MATERIAL

ITEM	UNIT	SUPER	SUB	TOTAL		
		_				

Descrip: Section thru integral abutment for PPC beams



# SECTION THRU INTEGRAL ABUTMENT

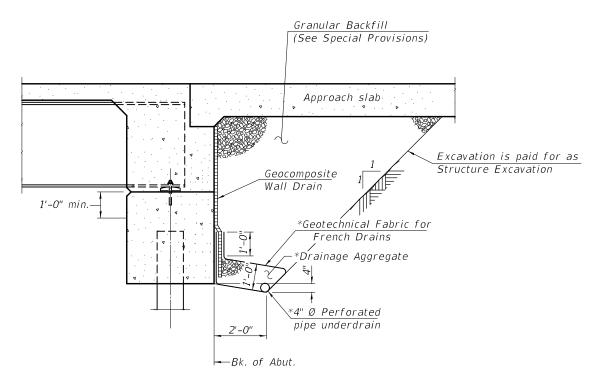
(Horiz. dim. @ Rt. L's)

\*Included in the cost of Pipe Underdrains for Structures. (See Special Provisions)

#### Note:

All drainage system components shall extend to 2'-0" from the end of each wingwall except an outlet pipe shall extend until intersecting with the side slopes. The pipes shall drain into concrete headwalls. (See Article 601.05 of the Standard Specifications and Highway Standard 601101).

Descrip: Section thru integral abutment for steel beams



## SECTION THRU INTEGRAL ABUTMENT

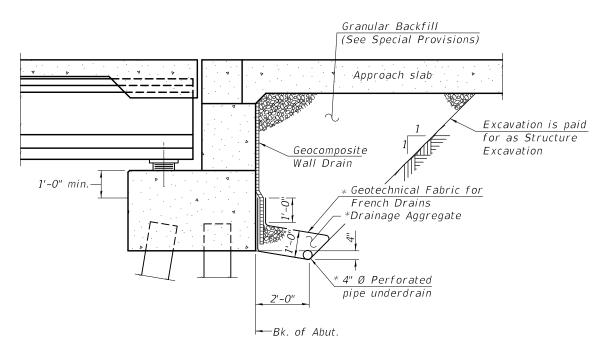
(Horiz. dim. @ Rt. Ľs)

\*Included in the cost of Pipe Underdrains for Structures. (See Special Provisions)

### Note:

All drainage system components shall extend to 2'-0" from the end of each wingwall except an outlet pipe shall extend until intersecting with the side slopes. The pipes shall drain into concrete headwalls. (See Article 601.05 of the Standard Specifications and Highway Standard 601101).

Descrip: Section thru pile supported stub abutment for PPC beams



# SECTION THRU PILE SUPPORTED

# STUB ABUTMENT

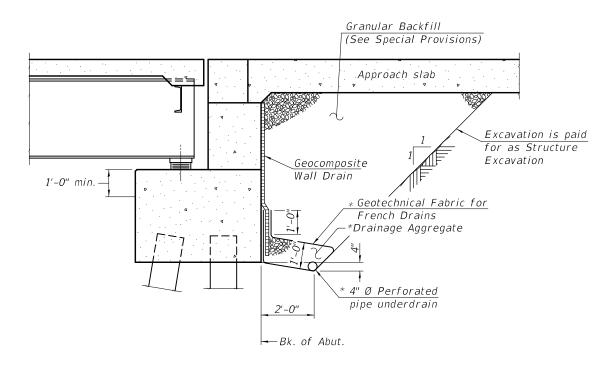
(Horiz. dim. @ Rt. L's)

\*Included in the cost of Pipe Underdrains for Structures. (See Special Provisions)

#### Note:

All drainage system components shall extend parallel to the abutment back wall until they intersect the wingwalls or 2'-0" from the end of the wingwalls when the wings are parallel to the abutment. The pipe shall extend under the wingwall, if necessary, until intersecting the side slopes. The pipes shall drain into concrete headwalls. (See Article 601.05 of the Standard Specifications and Highway Standard 601101).

Descrip: Section thru pile supported stub abutment for steel beams



### SECTION THRU PILE SUPPORTED STUB ABUTMENT

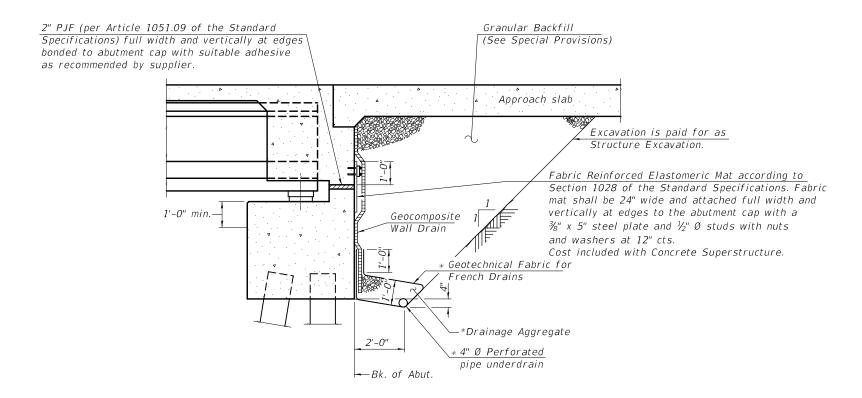
(Horiz. dim. @ Rt. L's)

\*Included in the cost of Pipe Underdrains for Structures. (See Special Provisions)

#### Note:

All drainage system components shall extend parallel to the abutment back wall until they intersect the wingwalls or 2'-0" from the end of the wingwalls when the wings are parallel to the abutment. The pipe shall extend under the wingwall, if necessary, until intersecting the side slopes. The pipes shall drain into concrete headwalls. (See Article 601.05 of the Standard Specifications and Highway Standard 601101).

Descrip: Section thru semi-integral abutment for PPC beams



## SECTION THRU SEMI-INTEGRAL ABUTMENT

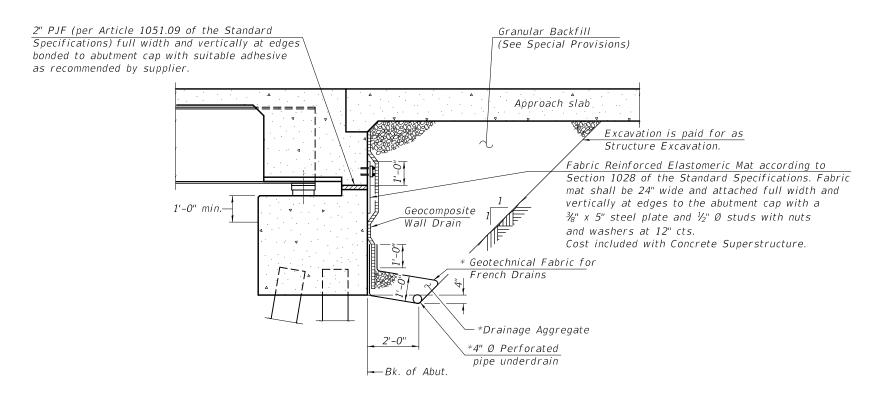
(Horiz. dim. @ Rt. L's)

\*Included in the cost of Pipe Underdrains for Structures. (See Special Provisions)

### Note:

All drainage system components shall extend to 2'-0" from the end of each wingwall except an outlet pipe shall extend until intersecting with the side slopes. The pipes shall drain into concrete headwalls. (See Article 601.05 of the Standard Specifications and Highway Standard 601101).

Descrip: Section thru semi-integral abutment for steel beams



## SECTION THRU SEMI-INTEGRAL ABUTMENT

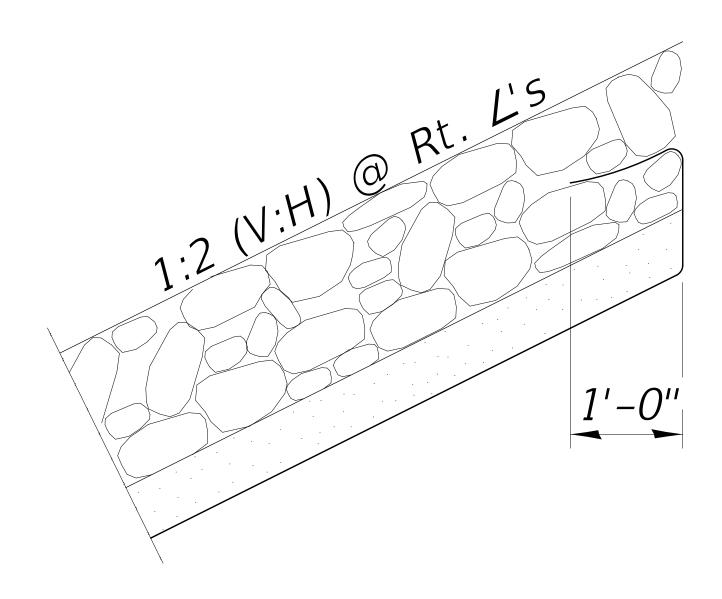
(Horiz. dim. @ Rt. L's)

\*Included in the cost of Pipe Underdrains for Structures. (See Special Provisions)

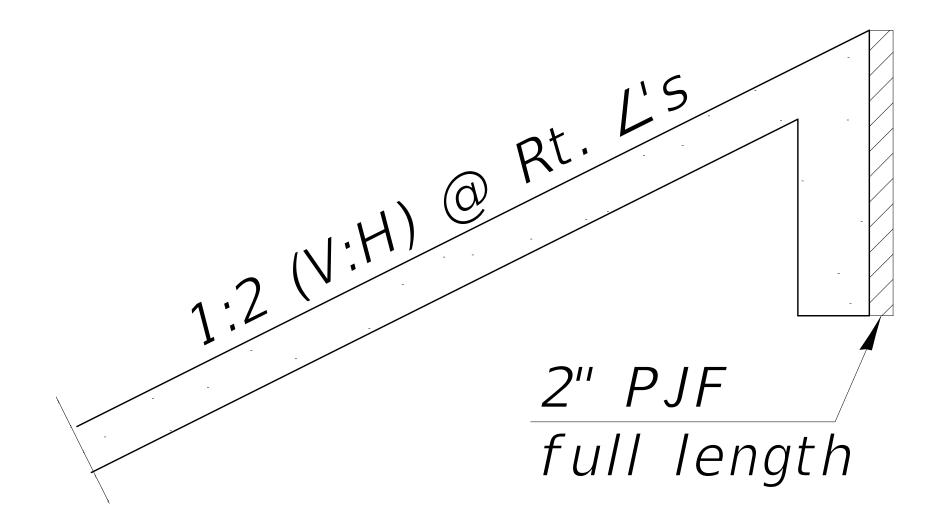
#### Note:

All drainage system components shall extend to 2'-0" from the end of each wingwall except an outlet pipe shall extend until intersecting with the side slopes. The pipes shall drain into concrete headwalls. (See Article 601.05 of the Standard Specifications and Highway Standard 601101).

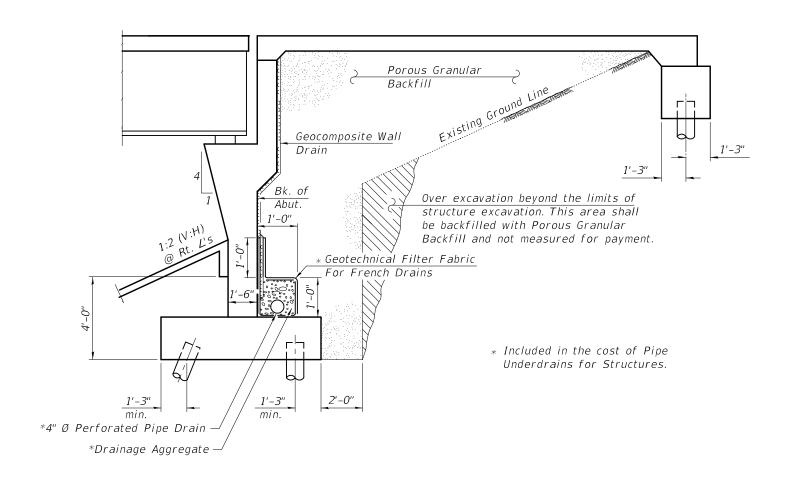
Descrip: Riprap for section thru abutments (use with D00010 through D00015)



Descrip: Slopewall for section thru abutments (use with D00010 through D00015)

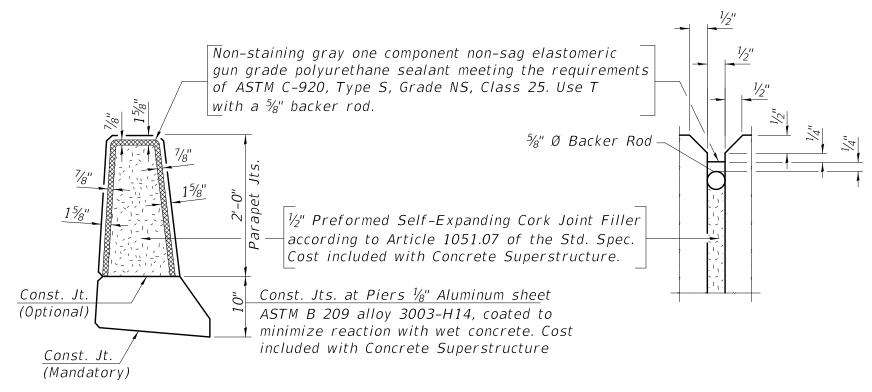


Descrip: Section Thru Filled Vaulted Abutment



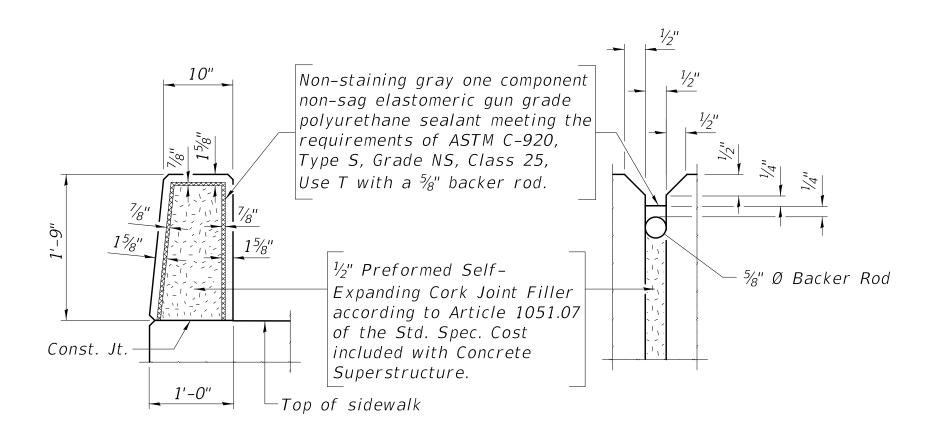
(Horiz. dim. @ Rt. Ľs)

Descrip: Parapet Joint Details



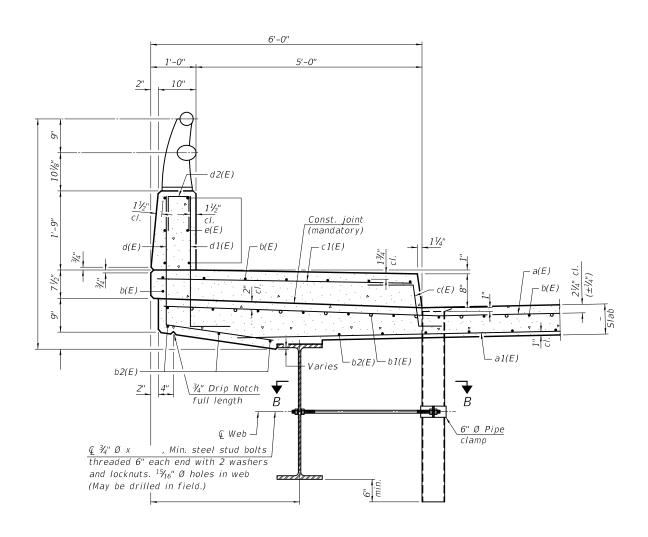
PARAPET JOINT DETAILS

Descrip: Parapet Joint at Sidewalk



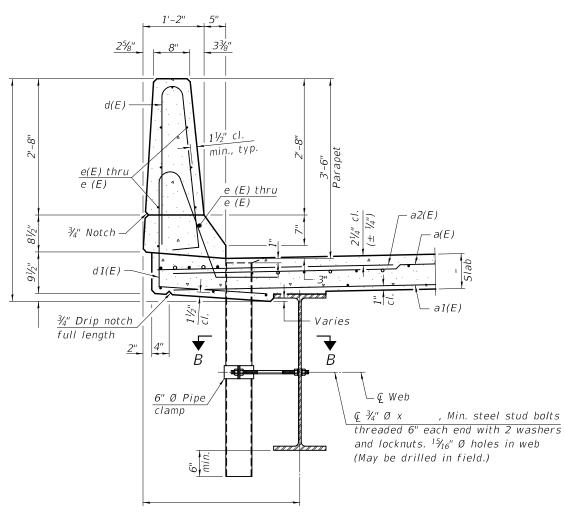
# PARAPET JOINT DETAILS

Descrip: Section thru sidewalk



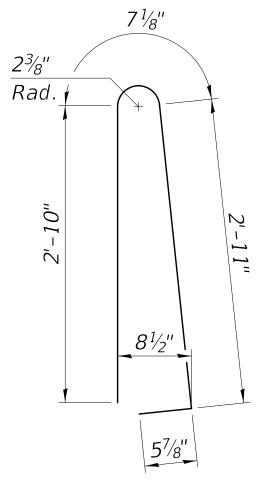
SECTION THRU SIDEWALK

Descrip: 42" Section thru parapet for base sheet S-D or S-I-D



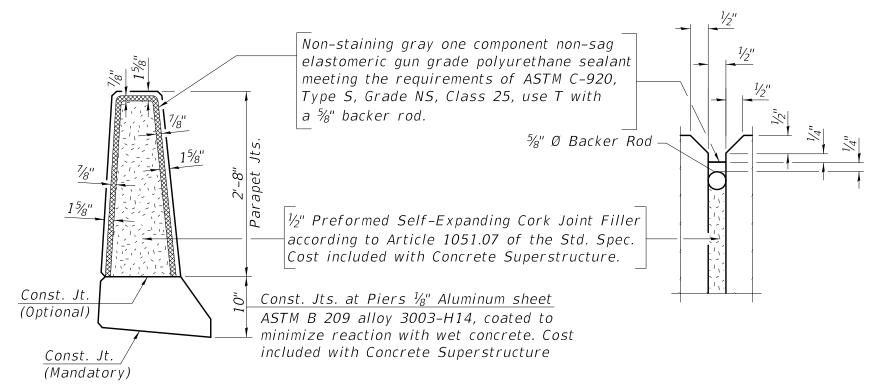
SECTION THRU PARAPET

Descrip: d(E) bar bending diagram for 42" parapet for base sheet S-D or S-I-D



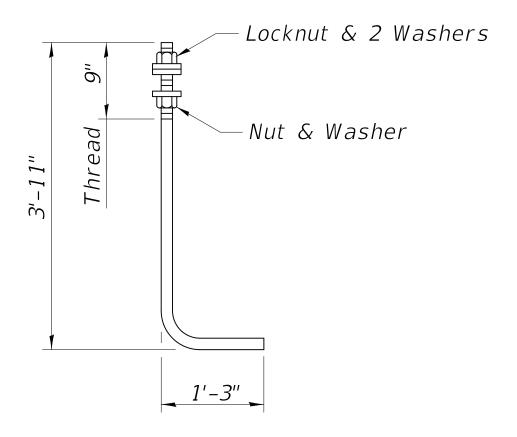
BAR d(E)

Descrip: 42" parapet joint details for base sheet S-D or S-I-D



PARAPET JOINT DETAILS

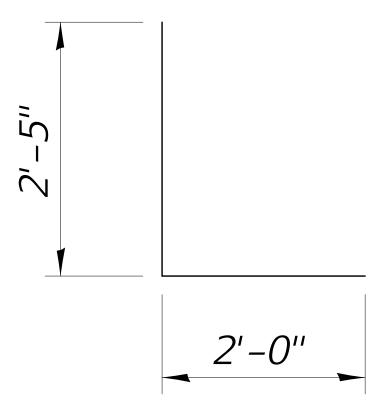
Descrip: Anchor rod for light pole mounted on parapet



ANCHOR ROD

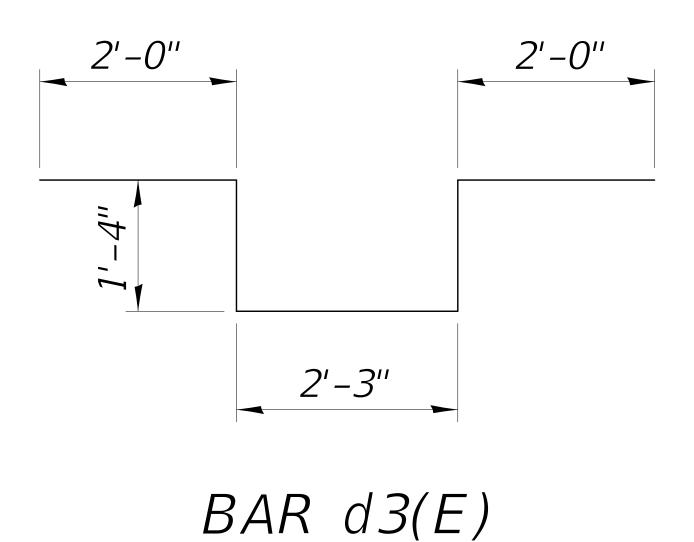
Diameter as specified for light poles. (ASTM F 1554 Grade 105)

Descrip: d2(E) bar bending diagram for parapet with light pole

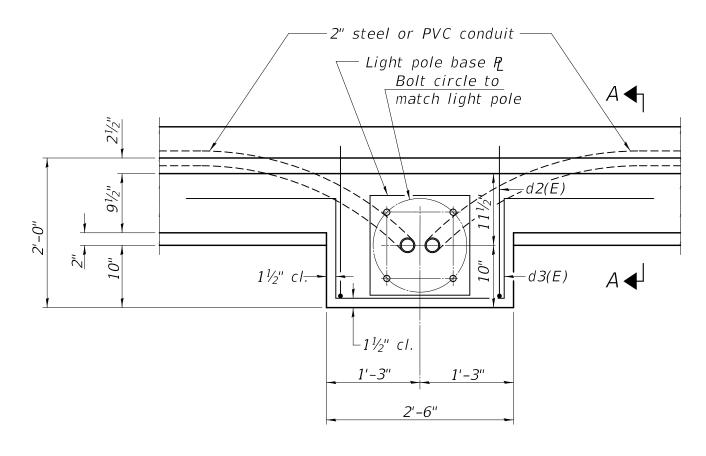


BAR d2(E)

Descrip: d3(E) bar bending diagram for parapet with light pole



Descrip: Plan view of parapet with light pole, conduit inside parapet

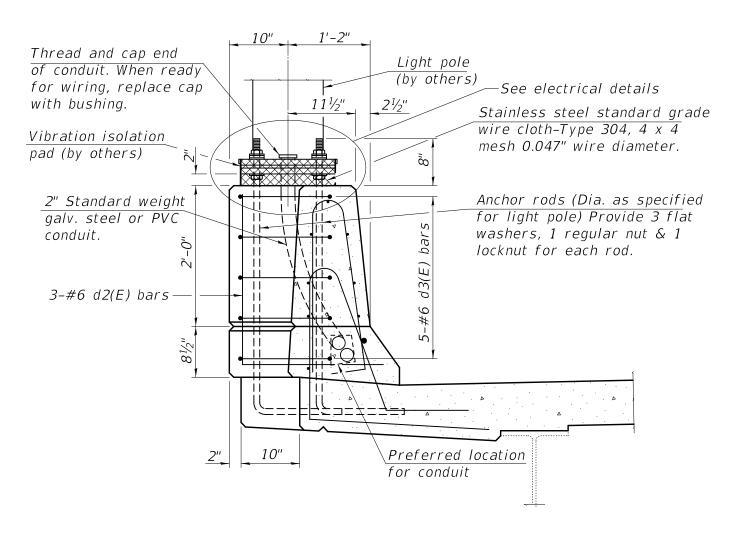


<u>PLAN</u>

Note:

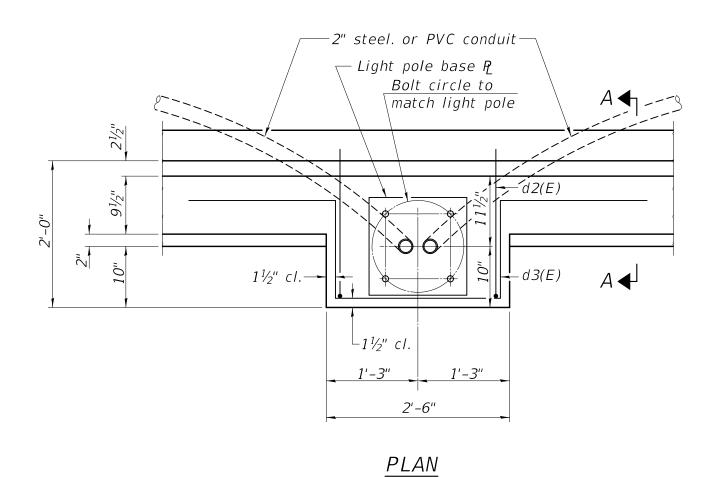
Cost of anchor rods and conduit is included with Concrete Superstructure.

Descrip: Section A-A of parapet with light pole, conduit inside parapet



SECTION A-A

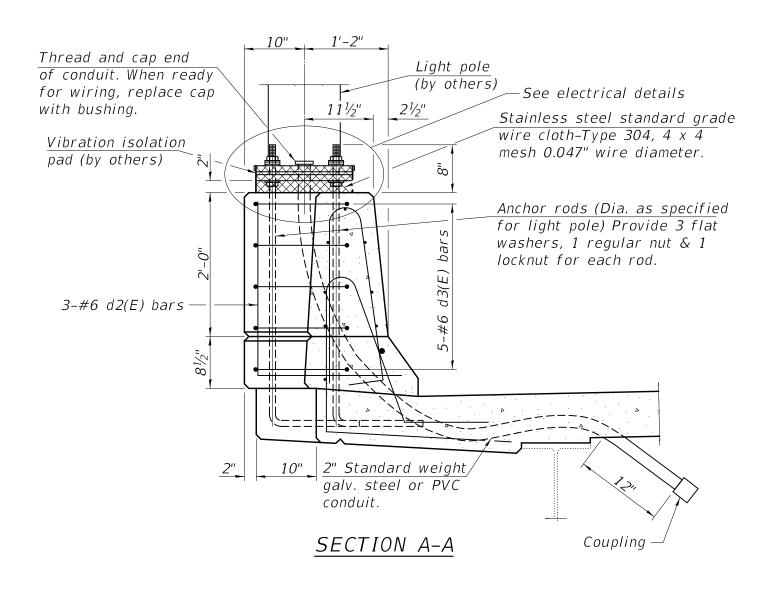
Descrip: Plan view of parapet with light pole, conduit outside parapet



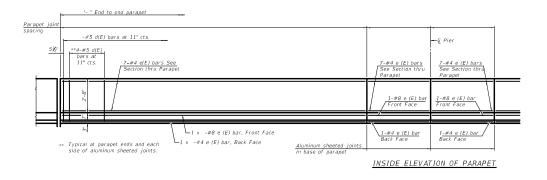
Note:

Cost of anchor rods and conduit is included with Concrete Superstructure.

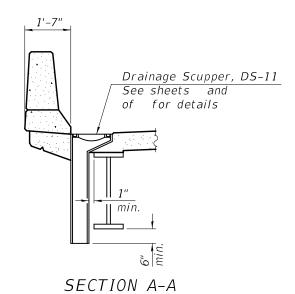
Descrip: Section A-A of parapet with light pole, conduit outside parapet

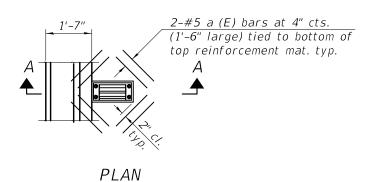


Descrip: Inside Elevation of 42" Parapet for superstructure detail sheet



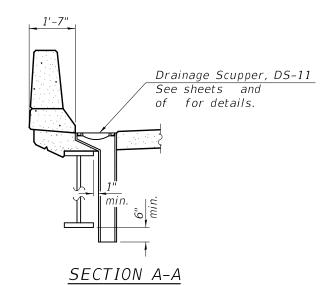
Descrip: Drainage Scupper, DS-11 details, left drain

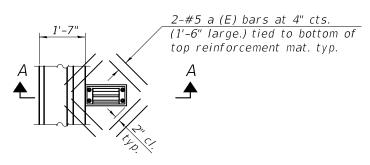




Note: Cut longitudinal reinforcement to clear drainage scuppers.

Descrip: Drainage Scupper, DS-11 details, right drain



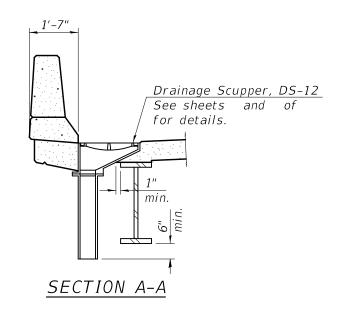


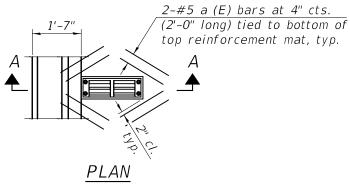
# PLAN

Note:

Cut longitudinal reinforcement to clear drainage scuppers.

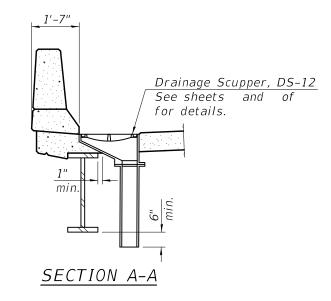
Descrip: Drainage Scupper, DS-12 details, left drain

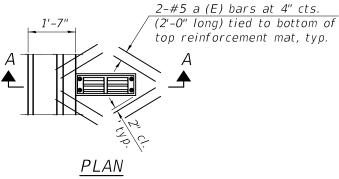




Note: Cut longitudinal reinforcement to clear drainage scuppers.

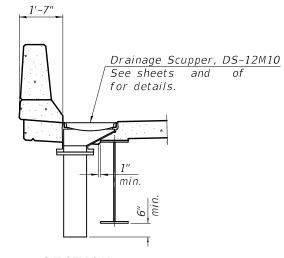
Descrip: Drainage Scupper, DS-12 details, right drain



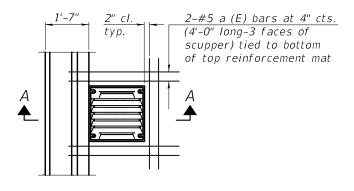


Note: Cut longitudinal reinforcement to clear drainage scuppers.

Descrip: Drainage Scupper, DS-12M10 details



## SECTION A-A

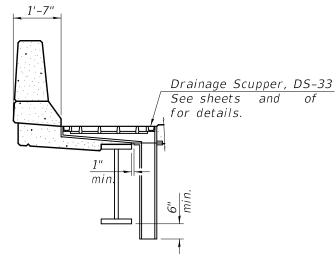


<u>PLAN</u>

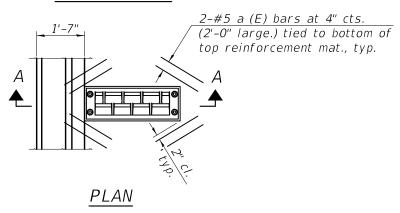
Note:

Cut longitudinal reinforcement to clear drainage scuppers.

Descrip: Drainage Scupper, DS-33 details, right drain

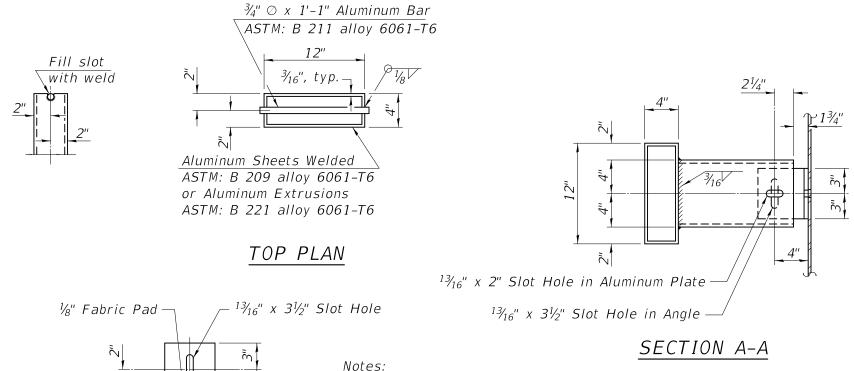


## SECTION A-A



Note: Cut longitudinal reinforcement to clear drainage scuppers.

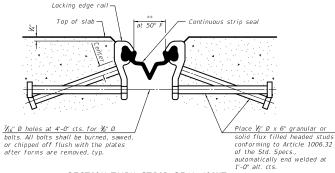
Descrip: 4 in x 12 in drain details



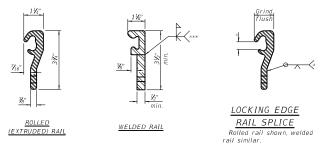
SECTION B-B

The exterior surfaces of the floor drains shall be painted with the finish coat as specified in the special provisions for Cleaning and Painting New Metal Structures. The exterior surfaces of the drain shall be cleaned and given a washcoat pretreatment in accordance with Society of Protective Coatings Spec. SSPC-SP1 & SSPC Paint 27 prior to painting.

Descrip: Strip seal joint for deck beams with CWS



#### <u>SECTION THRU STRIP SEAL JOINT</u> <u>FOR OVERLAY OVER DECK BEAMS</u>



#### LOCKING EDGE RAIL

- \* Omit weld at seal opening.
- \*\* The minimum dimension shall be 11/2"
- for installation purposes.
- \*\*\* Back gouge not required if complete joint penetration is verified by mock-up.

#### Notes

The strip seal shall be made continuous and shall have a minimum thickness of W. The configuration of the strip seal shall match the configuration of the Locking Edge Rails.

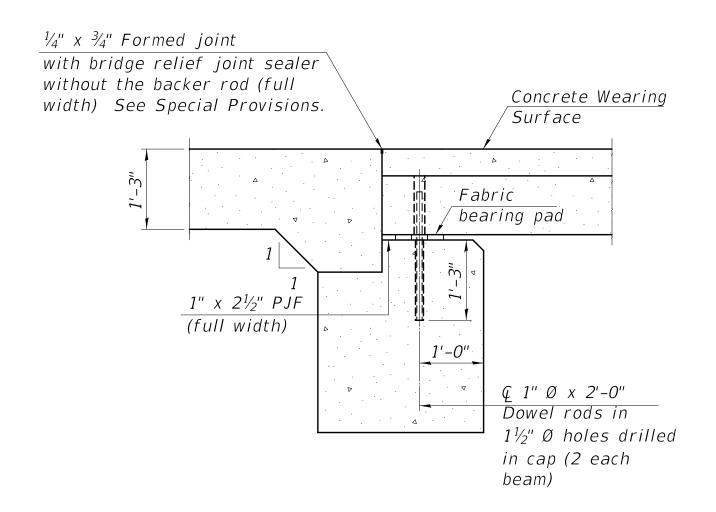
The height and thickness of the Locking Edge Rails shown are minimum dimensions. The actual configuration of the Locking Edge Rails and matching strip seal may vary from manufacturer to manufacturer. Flanged edge rails will not be allowed.

The inside of the Locking Edge Rail groove shall be free of weld residue. Locking Edge Rails may be spliced at slope discontinuities and stage construction joints.

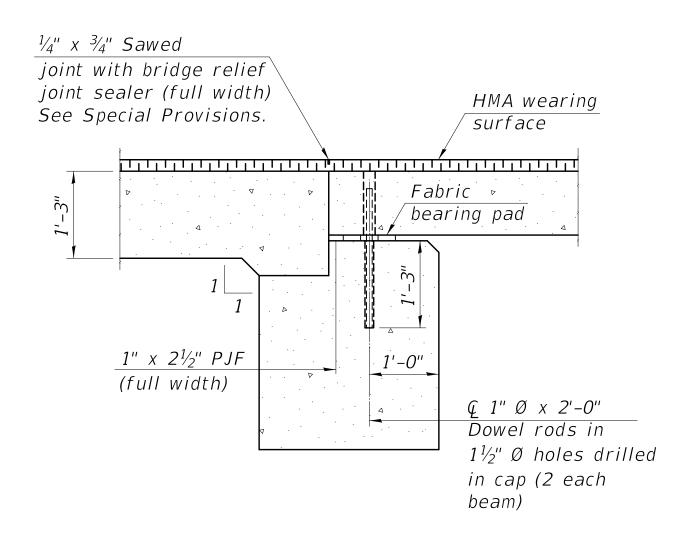
The manufacturer's recommended installation methods shall be followed. All steel components shall be galvanized after fabrication according to Article 520.03 of the Standard Specifications.

Maximum space between rail segments at stage lines shall be  $\sqrt[3]{_{16}}$ ", sealed with a suitable sealant

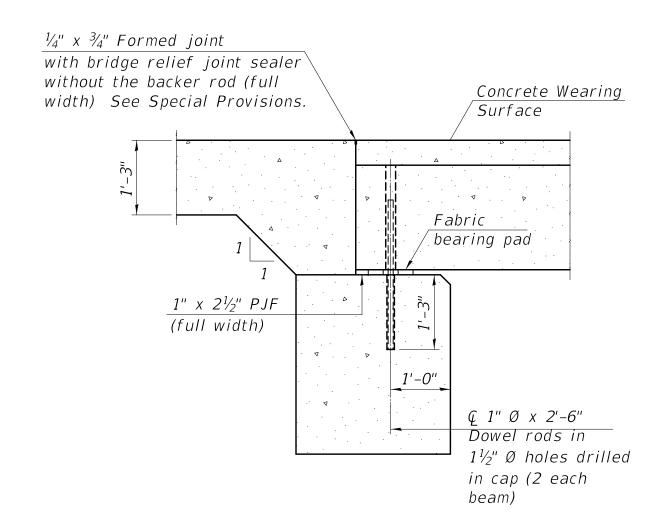
Descrip: Sect thru fixed abut for 11" PPC deck beam with conc. wearing surface and approach slab



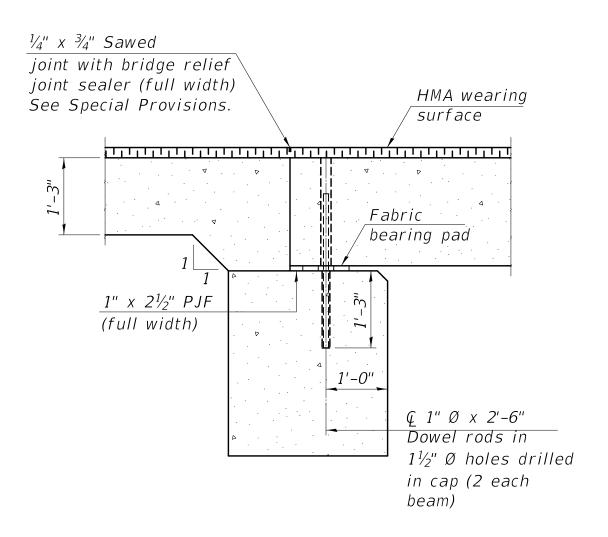
Descrip: Sect thru fixed abut. for 11" PPC deck beam with HMA wearing surface and approach slab



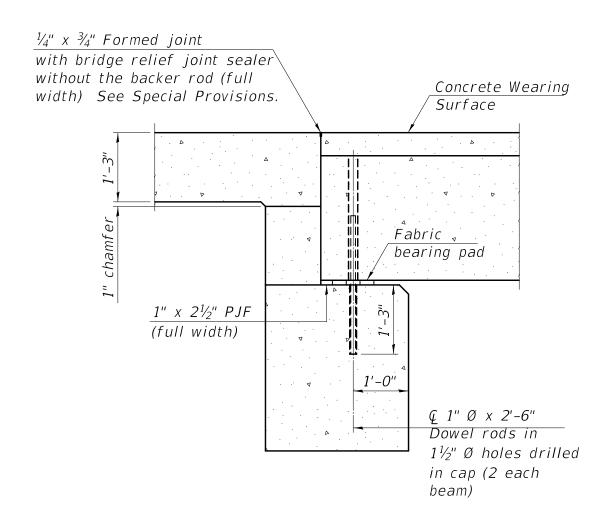
Descrip: Sect thru fixed abut. for 17" and 21" PPC deck beams with conc. wearing surface and approach slab



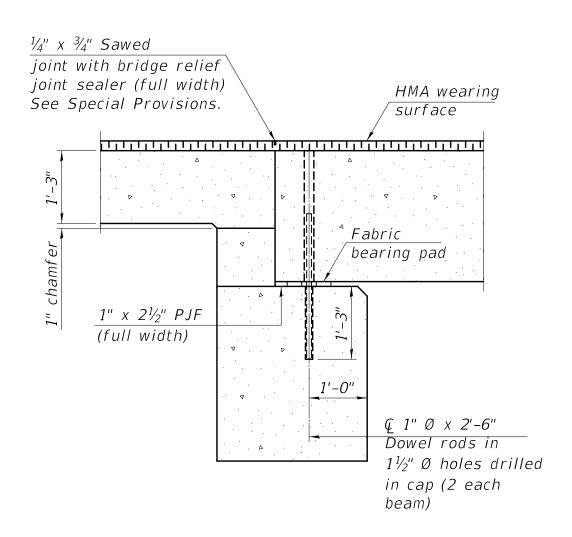
Descrip: Sect thru fixed abut. for 17" and 21" PPC deck beams with HMA wearing surface and approach slab



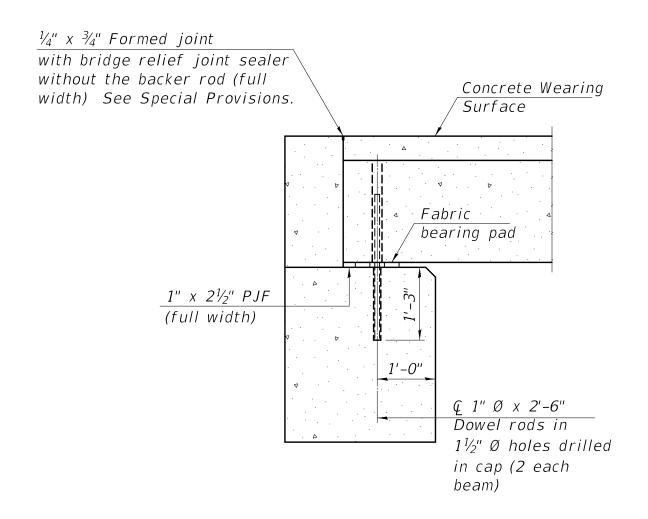
Descrip: Sect thru fixed abut. for 27", 33", and 42" PPC deck beams with conc. wearing surface and approach



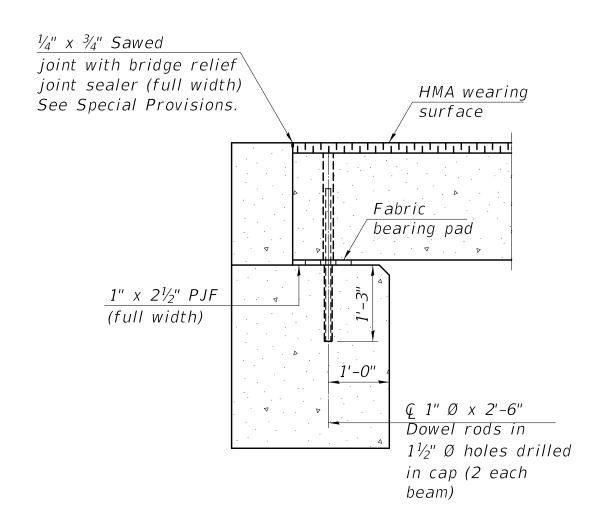
Descrip: Sect thru fixed abut. for 27", 33", and 42" PPC deck beams with HMA wearing surface and approach



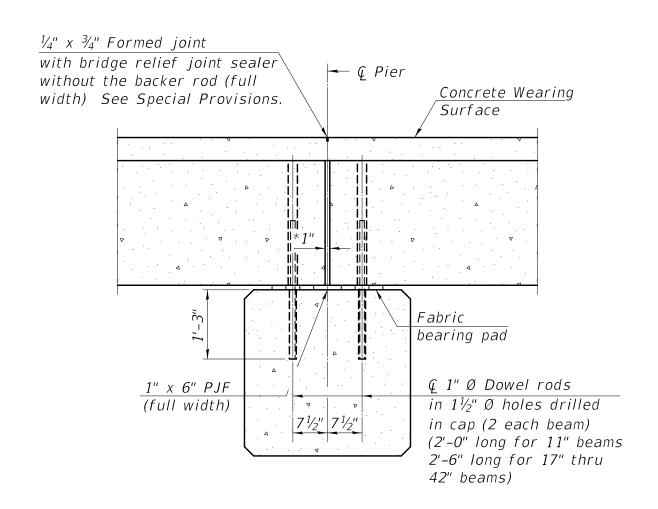
Descrip: Sect thru fixed abut. for 11" thru 42" PPC deck beams with conc. wearing surface without approach



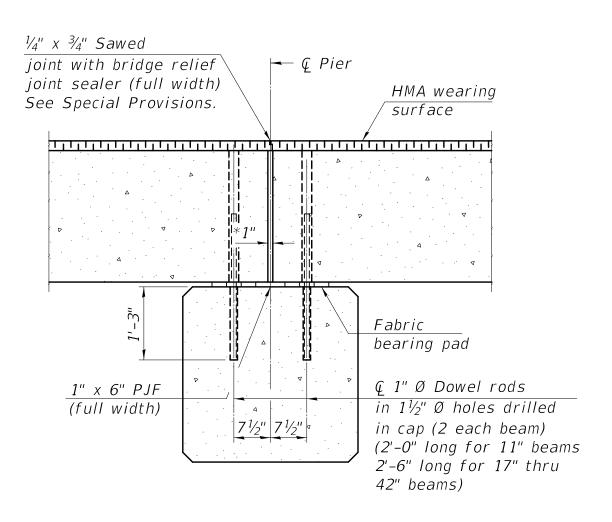
Descrip: Sect thru fixed abut. for 11" thru 42" PPC deck beams with HMA wearing surface without approach



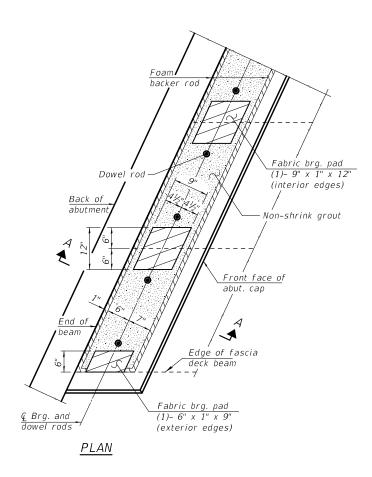
Descrip: Sect thru fixed pier for 11" thru 42" PPC deck beams with concrete wearing surface



Descrip: Sect thru fixed pier for 11" thru 42" PPC deck beams with HMA wearing surface



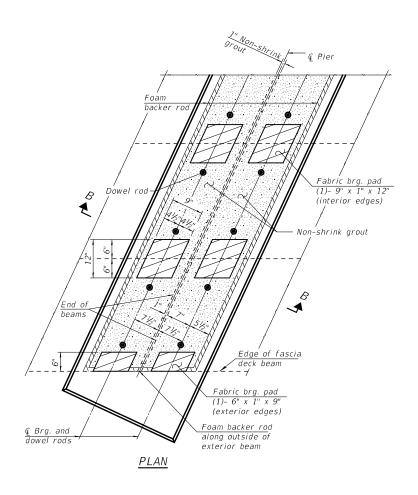
Descrip: Plan View of alternate fixed bearings at abutments



#### Notes

The bearing seat surfaces shall be adjusted by shimming the bearing to assure firm and even bearing prior to placement of grout.  $2-V_8''$  fabric adjusting shims of the dimensions of the exterior bearing pad shown shall be provided for each bearing.

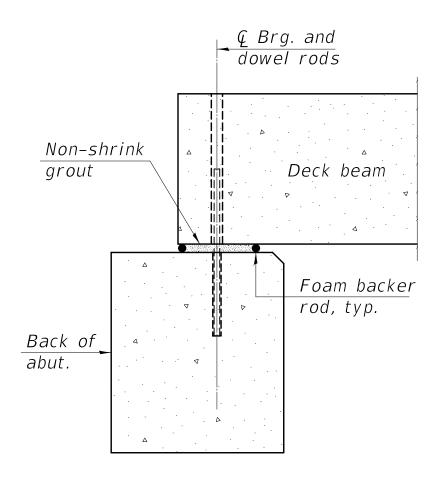
Descrip: Plan View of alternate fixed bearings at pier



#### Notes

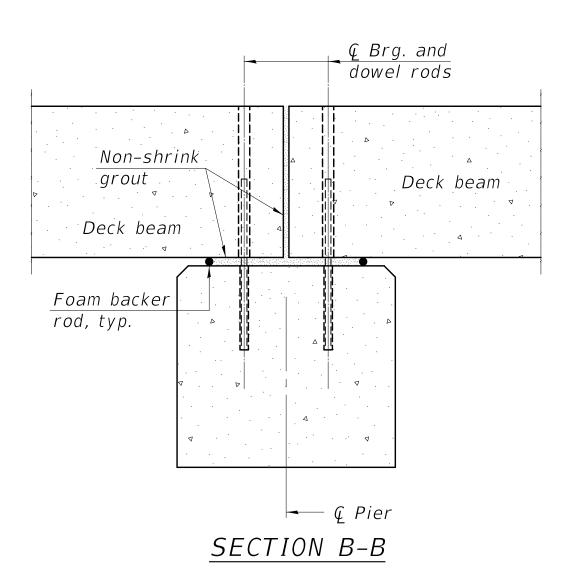
The bearing seat surfaces shall be adjusted by shimming the bearing to assure firm and even bearing prior to placement of grout.  $2-V_0^{\mu}$  fabric adjusting shims of the dimensions of the exterior bearing pad shown shall be provided for each bearing.

Descrip: Sect thru fixed abut. with alternate fixed bearings

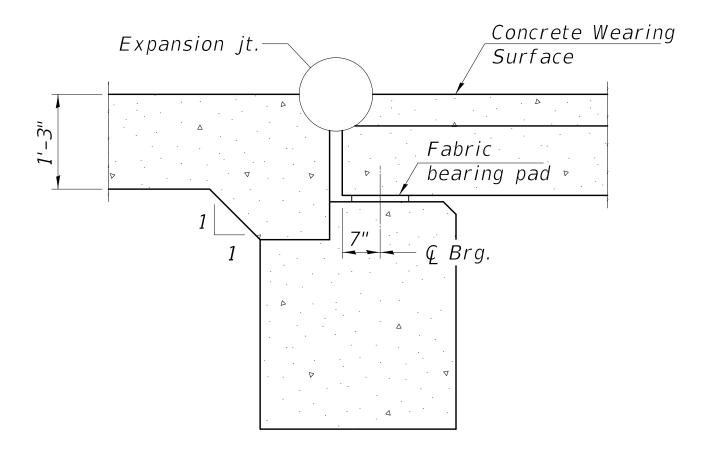


SECTION A-A

Descrip: Sect thru fixed pier with alternate fixed bearings



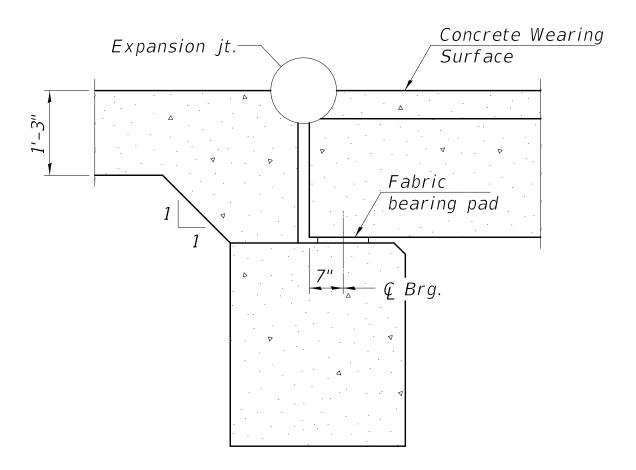
Descrip: Sect thru expansion abut. for 11" PPC deck beams with conc. wearing surface



# SECTION THRU ABUTMENT (Dimensions are at Rt. L's)

Descrip: Sect thru expansion abut. for 17" and 21" PPC deck beams with conc. wearing surface and approach

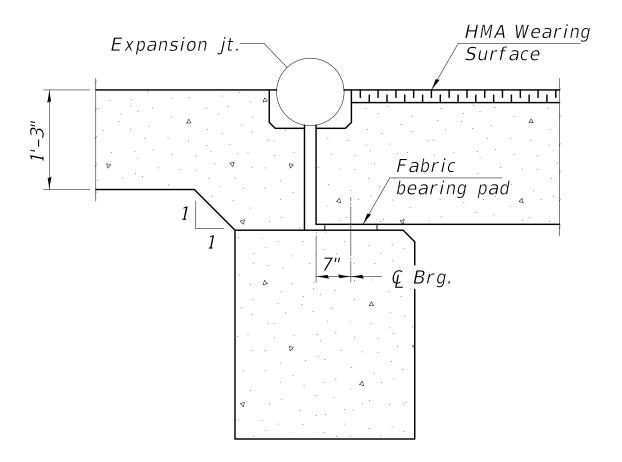
slab



## SECTION THRU ABUTMENT

Descrip: Sect thru expansion abut. for 17" and 21" PPC deck beams with HMA wearing surface and approach

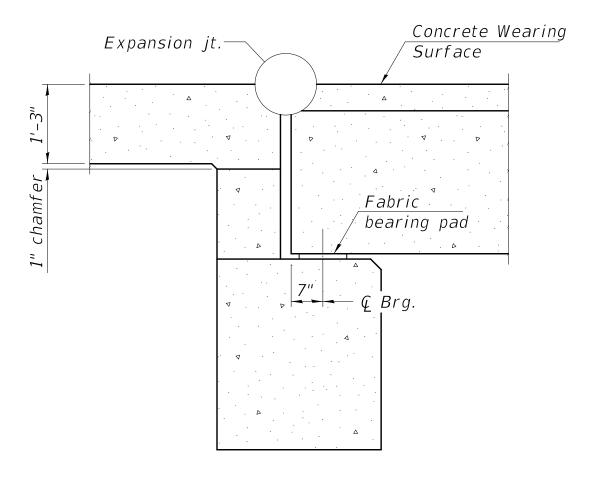
slab



## SECTION THRU ABUTMENT

Descrip: Sect thru expansion abut. for 27", 33", and 42" PPC deck beams with conc. wearing surface and

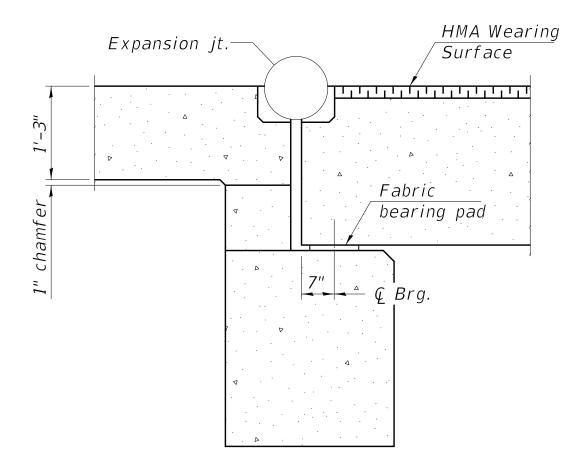
approach slab



## SECTION THRU ABUTMENT

Descrip: Sect thru expansion abut. for 27", 33", and 42" PPC deck beams with HMA wearing surface and

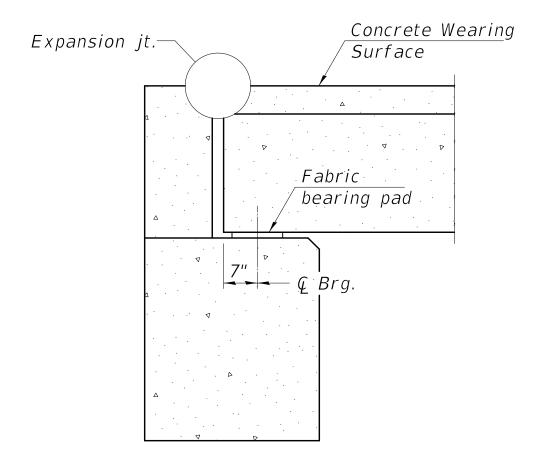
approach slab



## SECTION THRU ABUTMENT

Descrip: Sect thru expansion abut. for 11" thru 42" PPC deck beams with conc. wearing surface without

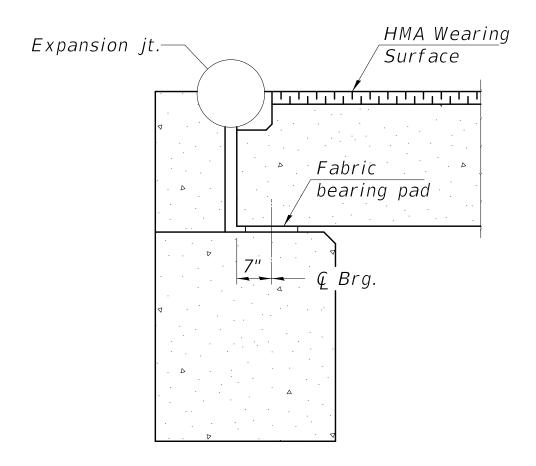
approach slab



## SECTION THRU ABUTMENT

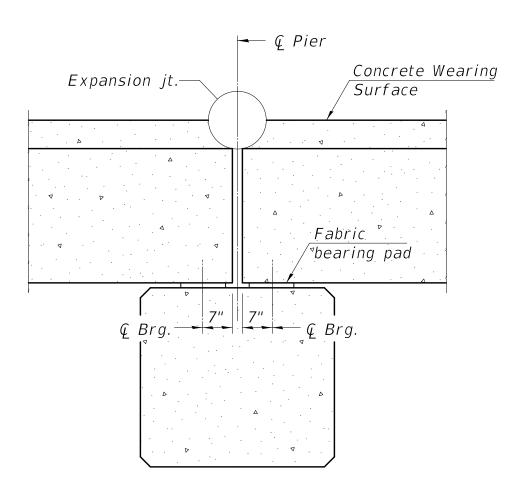
Descrip: Sect thru expansion abut. for 17" thru 42" PPC deck beams with HMA wearing surface without

approach slab



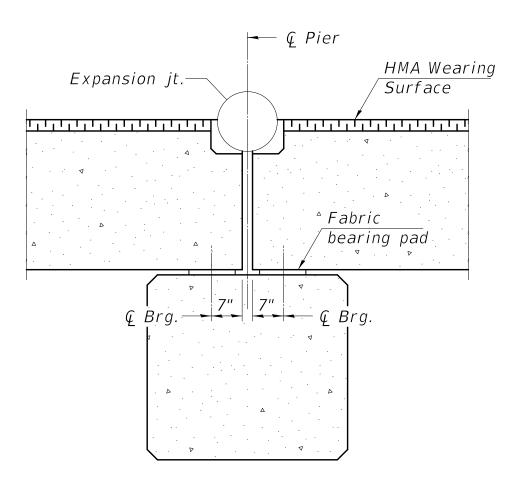
## SECTION THRU ABUTMENT

Descrip: Sect thru expansion pier for 11" thru 42" PPC deck beams with conc. wearing surface



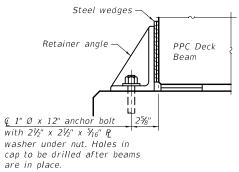
SECTION THRU PIER

Descrip: Sect thru expansion pier for 17" thru 42" PPC deck beams with HMA wearing surface

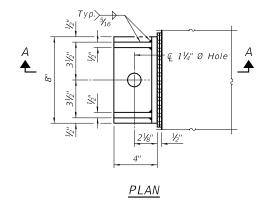


SECTION THRU PIER (Dimensions are at Rt. L's)

Descrip: Retainer angle at expansion joint of deck beams



### SECTION A-A



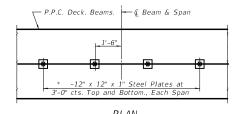
#### Notes:

Cost of retainer and accessories are included with Precast Prestressed Concrete Deck Beams. Equivalent rolled angle with stiffeners will be allowed in lieu of welded plates.

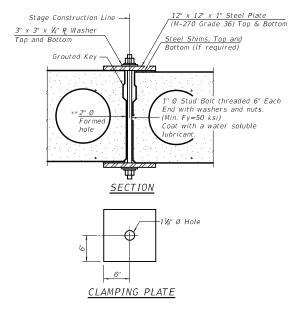
The side retainers shall be galvanized after shop fabrication according to AASHTO M 111 and ASTM 385. Anchor bolts and plate washers shall be galvanized according to AASHTO M 232.

After the notch or concrete overlay are poured and cured, the steel wedges shall be removed.

Descrip: Shear key clamping details at stage construction joint



\*Space plates to miss Temporary Bridge Rail Posts.

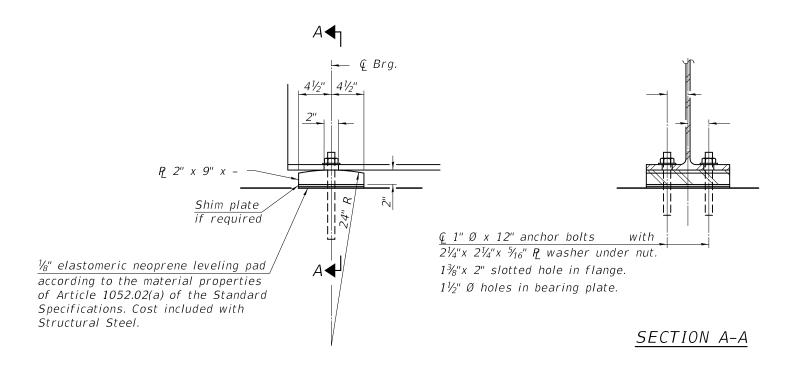


#### SHEAR KEY CLAMPING DETAILS AT STAGE CONST. JT.

Cost included with Precast Prestressed Concrete Deck Beams. See Stage Construction Details for traffic lanes.

\*\* Cast semicircular recesses in the sides of each beam adjacent to the stage construction line. These recesses should align to form a hole at the appropriate locations for the clamping device bolts.

Descrip: Bearing detail for integral abutment with steel beams



## ELEVATION AT ABUTMENT

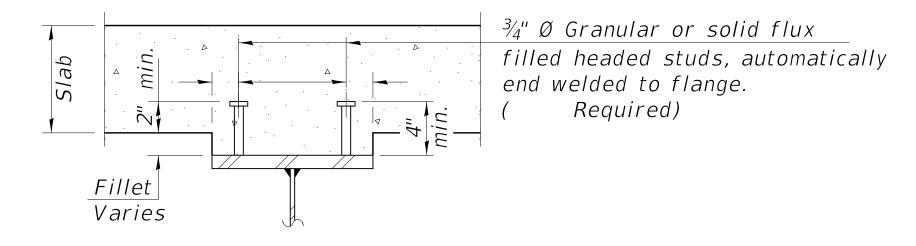
### FIXED BEARING

Notes:

Anchor bolts shall be according to Article 521.06 of the Standard Specifications. Beams shall be braced for stability during erection and remain braced until deck is poured and cured.

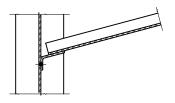
Anchor bolts at all supports shall be installed as each member is erected unless an equivalent temporary means of lateral restraint is used.

Descrip: Stud shear connector details

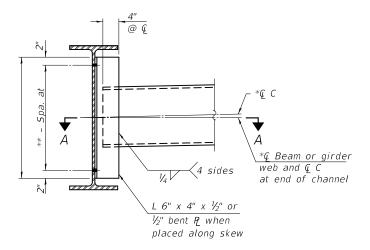


SECTION A-A

Descrip: Interior diaphragm beam or girder up to 42"



### SECTION A-A



### INTERIOR DIAPHRAGM

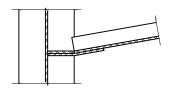
Note

Two hardened washers required for each set of oversized holes.

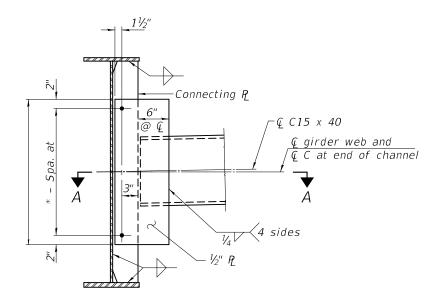
\*Alternate channels are permitted to facilitate material acquisition. Calculated weight of structural steel is based on the lighter section.

The alternate, if utilized, shall be provided at no additional cost to the Department. \*\* $\frac{3}{4}$ " Ø HS bolts,  $\frac{15}{16}$ " Ø holes

Descrip: Interior diaphragm plate girder < 48"



## SECTION A-A

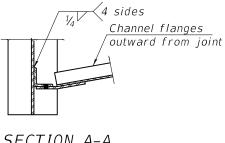


### INTERIOR DIAPHRAGM

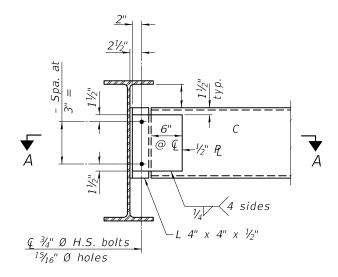
Note:

Two hardened washers required for each set of oversized holes. \* $^{15}\!\!/_{16}$ " Ø holes

Descrip: End diaphragm for wide flange beams



## SECTION A-A

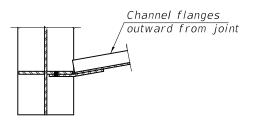


## END DIAPHRAGM

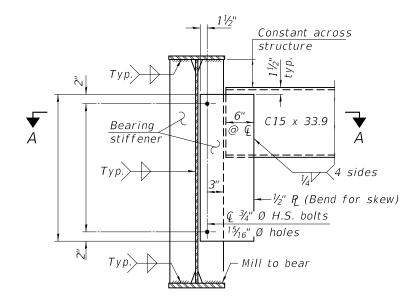
Note:

Two hardened washers required for each set of oversized holes.

Descrip: End diaphragm for shallow plate girders



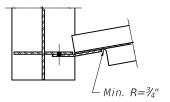
## SECTION A-A



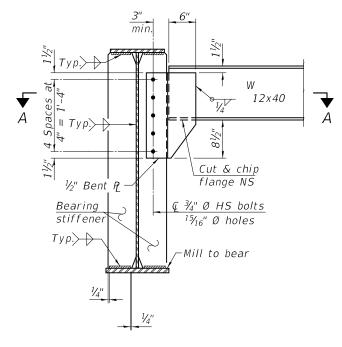
## Note: END DIAPHRAGM

Two hardened washers required for each set of oversized holes.

Descrip: End diaphragm for plate girders < 48" and skew < 45 deg with finger plate or modular joints



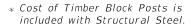
## SECTION A-A

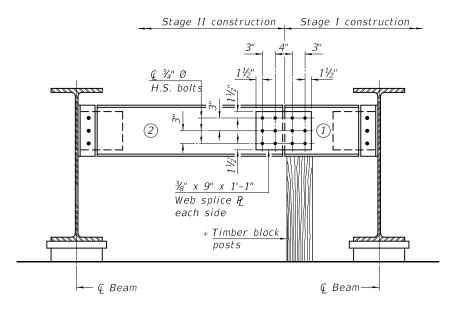


## END DIAPHRAGM

Note: Two hardened washers required for each set of oversized holes.

Descrip: End diaphragm stage construction sequence for wide flange beams





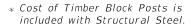
## END DIAPHRAGM

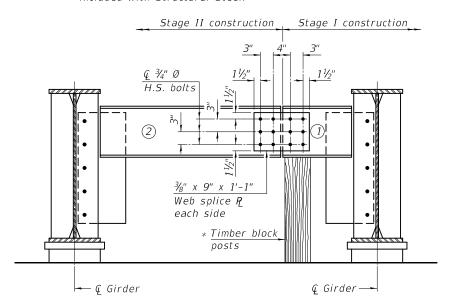
## END DIAPHRAGM STAGE CONSTRUCTION SEQUENCE

Order diaphragm in two sections.

- 1.) Attach section 1 of diaphragm to beam
- 2.) Place timber block posts between section (1) of diaphragm and
- 3.) abutment bearing section.
- 4.) Attach section (2) of diaphragm to both beam and section (1)
- 5.) of diaphragm during stage II construction with splice plates. Remove timber block posts.

Descrip: End diaphragm stage construction sequence for plate girders





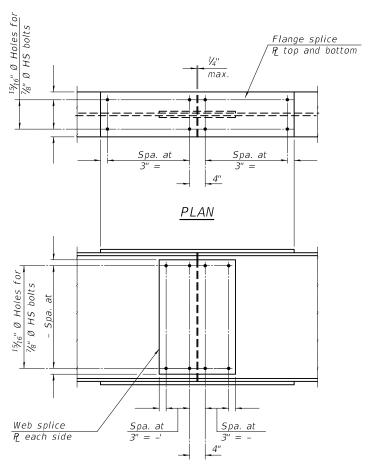
## END DIAPHRAGM

# END DIAPHRAGM STAGE CONSTRUCTION SEQUENCE

Order diaphragm in two sections.

- 1.) Attach section ① of diaphragm to girder
- 2.) Place timber block posts between section (1) of diaphragm and
- 3.) abutment bearing section.
- 4.) Attach section (2) of diaphragm to both girder and section (1)
- 5.) of diaphragm during stage II construction with splice plates. Remove timber block posts.

Descrip: Wide flange splice detail (outside flange plates only)



ELEVATION

SPLICE DETAIL
( Required)

Descrip: LRFD data tables (Non-composite in negative moment regions)

INTERIOR GIRDER MOMENT TABLE   0.4 Sp. 1 or 0.6 Sp. 2   Pier							
Is (in <sup>4</sup> ) Ic(n) (in <sup>4</sup> ) Ic(3n) (in <sup>4</sup> ) Ss (in <sup>3</sup> ) Sc(n) (in <sup>3</sup> ) Sc(n) (in <sup>3</sup> ) Sc(3n) (in <sup>3</sup> ) DC1 (k/) MDC1 (k/) MDC2 (k) MDC2 (k/) MDW (k/) MDW (k/) Mbw (k/) Mbw (k/) Mbw (k/) Mbw (k/) Mbw (k/) Mcontain (k) Mcont	INTER.	IOR GIE					
Ic(n) (in <sup>4</sup> ) Ic(3n) (in <sup>4</sup> ) Ss (in <sup>2</sup> ) Sc(n) (in <sup>3</sup> ) Sc(3n) (in <sup>3</sup> ) Sc(3n) (in <sup>3</sup> ) DC1 (k/) MDC1 (k) DC2 (k/) MDC2 (k) DW (k/) MDW (k/) MW (k/) MW (Strength I) (k) Ms DC1 (ksi) fs DC1 (ksi) fs DC2 (ksi) fs SC1 (ksi) fs (Service II) (ksi) O.95Rh Fyf (ksi) In (in <sup>4</sup> ) Is (in <sup>4</sup>			0.4 Sp	. 1 or	0.6 .	Sp. 2	Pier
Ic(3n)							
Ss     (in³)       Sc(n)     (in³)       Sc(3n)     (in³)       DC1     (k/r)       MDC1     ('k)       DC2     (k/r)       MDC2     ('k)       DW     (k/r)       MDW     ('k)       Mty     ('k)       Mu (Strength I)     ('k)       Øf Mn     ('k)       fs DC1     (ksi)       fs DC2     (ksi)       fs DW     (ksi)       fs (½+IM)     (ksi)       fs (Service II)     (ksi)       fs (Total)(Strength I) (ksi)     (fsi)       Øf Fn     (ksi)							
Sc(n) (in³) Sc(3n) (in³) DC1 (k/) MDC1 (k/) MDC2 (k/) MDC2 (k/) MDW (k/) MDW (k/) ML (Strength I) (k) MS DC2 (kSi) MS DC2 (kSi) MS DC1 (kSi) MS DC2 (kSi) MS DC3 (kSi) MS DC4 (kSi) MS DC5 (kSi) MS DC5 (kSi) MS DC6 (kSi) MS DC7 (kSi) MS DC8 (kSi) MS DC9		(in⁴)					
Sc(3n) (in³) DC1 (k/r) MDC1 (k/r) MDC2 (k/r) MDC2 (k/r) MDW (k/r) MDW (k/r) ML + IM (k) ML (Strength I) (k) Mf + DC2 (ksi) Mf + DC2 (ksi) Mf + DC2 (ksi) Mf + DC3 (ksi) Mf + DC4 (ksi) Mf + DC5 (ksi) Mf + DC5 (ksi) Mf + DC6 (ksi) Mf + DC7 (ksi) Mf + DC8 (ksi) Mf + DC8 (ksi) Mf + DC9 (ksi) Mf	Ss	(in³)					
DC1 (k/') MDC1 ('k') DC2 (k/') MDC2 (k/') MDC2 ('k) DW (k/') MDW (k/') ML + IM ('k) Mu (Strength I) ('k) Øf Mn ('k) fs DC1 (ksi) fs DC2 (ksi) fs DW (ksi) fs (t+IM) (ksi) fs (Service II) (ksi) fs (Service III) (ksi) O.95Rh Fyf (ksi) fs (Total)(Strength I)(ksi) Øf Fn (ksi)	Sc(n)	(in³)					
MDC1 ('k) DC2 (k/') MDC2 (k') DW (k/') MDW (k') MU (Strength I) ('k) Mu (Strength I) ('k) fs DC1 (ksi) fs DC2 (ksi) fs DC2 (ksi) fs DW (ksi) fs (\(\frac{t}{t}\)HM (ksi) fs (Service II) (ksi) 0.95Rh Fyf (ksi) fs (Total)(Strength I)(ksi) Of Fn (ksi)	Sc(3n)	(in³)					
DC2 (k/') MDC2 (k) DW (k/') MDW (k/') MDW (k) ML + IM ('k) MU (Strength I) (k) MF DC1 (ksi) FS DC2 (ksi) FS DC2 (ksi) FS DW (ksi) FS (\(\frac{1}{2}\) HM) (ksi) FS (Service II) (ksi) O.95Rh Fyf (ksi) FS (Total)(Strength I)(ksi) Of Fn (ksi)	DC1	(k/')					
MDC2 ('k)  DW (k/')  MDW (k/')  ML + 1M ('k)  ML + 1M ('k)  MI (Strength I) ('k)  Øf Mn ('k)  fs DC1 (ksi)  fs DC2 (ksi)  fs DW (ksi)  fs (\frac{1}{2} \text{K} \text{K} \text{K} \text{S} \text{I}  fs (\frac{1}{2} \text{K} \text{II}) (ksi)  fs (\frac{1}{2} \text{Crotal}) (ksi)  fs (\frac{1}{2} \text{Crotal}) (ksi)  Øf Fn (ksi)	MDC1	('k)					
DW (k/') MDW (k)  ML + IM ('k)  M t (Strength I) ('k)  Of Mn ('k)  fs DC1 (ksi)  fs DC2 (ksi)  fs DW (ksi)  fs (L+IM) (ksi)  fs (Service II) (ksi)  O.95Rh Fyf (ksi)  Of Fn (ksi)  Of Fn (ksi)		(k/')					
MDW ('k)  Mt_+ IM ('k)  Mu (Strength I) ('k)  Øf Mn ('k)  fs DC1 (ksi)  fs DC2 (ksi)  fs DW (ksi)  fs (t+IM) (ksi)  fs (Service II) (ksi)  0.95Rh Fyf (ksi)  Øf Fn (ksi)  Øf Fn (ksi)	MDC2	('k)					
Mt + IM ('k) Mu (Strength I) ('k) Øf Mn ('k) fs DC1 (ksi) fs DC2 (ksi) fs DW (ksi) fs (t+IM) (ksi) fs (Service II) (ksi) Øf S(Total)(Strength I)(ksi) Øf Fn (ksi)	DW	(k/')					
Mu (Strength I) ('k)  Øf Mn ('k)  fs DC1 (ksi)  fs DC2 (ksi)  fs DW (ksi)  fs (\(\frac{t}{+}\)IM) (ksi)  fs (\(\frac{t}{+}\)IM) (ksi)  fs (Service II) (ksi)  0.95Rh Fyf (ksi)  Øf Fn (ksi)  Øf Fn (ksi)	MDW	('k)					
Øf Mn     ('k)       fs DC1     (ksi)       fs DC2     (ksi)       fs DW     (ksi)       fs (½+IM)     (ksi)       fs (Service II)     (ksi)       0.95Rh Fyf     (ksi)       fs (Total)(Strength I) (ksi)     (fsi)       Øf Fn     (ksi)	MŁ + IM	('k)					
fs DC1     (ksi)       fs DC2     (ksi)       fs DW     (ksi)       fs (\text{t-IM})     (ksi)       fs (Service II)     (ksi)       0.95Rh Fyf     (ksi)       fs (Total)(Strength I) (ksi)     (friction of the content of the cont							
fs DC2 (ksi) fs DW (ksi) fs (t+IM) (ksi) fs (Service II) (ksi) 0.95Rh Fyf (ksi) fs (Total)(Strength I) (ksi) Øf Fn (ksi)		('k)					
fs DW (ksi) fs (\(\frac{t}{+}\)IM) (ksi) fs (Service II) (ksi) 0.95Rh Fyf (ksi) fs (Total)(Strength I) (ksi) Øf Fn (ksi)							
fs (\(\frac{1}{2}\)HM) (ksi) fs (Service II) (ksi) 0.95Rh Fyf (ksi) fs (Total)(Strength I) (ksi) Øf Fn (ksi)	fs DC2	(ksi)					
fs (Service II) (ksi) 0.95Rh Fyf (ksi) fs (Total)(Strength I) (ksi) Øf Fn (ksi)	fs DW						
0.95Rh Fyf (ksi) fs (Total)(Strength I) (ksi) Øf Fn (ksi)	fs (½+IM)	(ksi)					
fs (Total)(Strength I) (ksi) Øf Fn (ksi)							
Øf Fn (ksi)							
		I) (ksi)					
Vf (k)							
	Vf	(k)					

INTERIOR GI	RDER REACT.	ION TABLE
	Abut.	Pier
RDC1 (k	)	
RDC2 (k	)	
RDW (k	)	
RL+IM (k	)	
RTotal (k	)	

Is, Ss: Non-composite moment of inertia and section modulus of the steel section used for computing fs(Total-Strength I, and Service II) due to non-composite dead loads (in.4 and in.3).

Ic(n), Sc(n): Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing fs(Total-Strength I, and Service II) due to short-term composite live loads (in.4 and in.3).

Ic(3n), Sc(3n): Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing fs(Total-Strength I, and Service II) due to long-term composite (superimposed) dead loads (in.4 and in.3).

DC1:Un-factored non-composite dead load (kips/ft.).

MDC1: Un-factored moment due to non-composite dead load (kip-ft.).

DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

MDW: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).

M + i m: Un-factored live load moment plus dynamic load allowance (impact) (kip-ft.).

Mu (Strength I): Factored design moment (kip-ft.).

1.25 (MDC1 + MDC2) + 1.5 MDW + 1.75 M\( \) + IM

Of Mn: Compact composite positive moment capacity computed according to Article 6.10.7.1 or non-slender negative moment capacity according to Article A6.1.1 or A6.1.2 (kip-ft).

fs DC1: Un-factored stress at edge of flange for controlling steel flange due to vertical non-composite dead loads as calculated below (ksi). MDC1 / Snc

fs DC2: Un-factored stress at edge of flange for controlling steel flange due to vertical composite dead loads as calculated below (ksi).

MDC2 / Sc(3n) or MDC2 / Sc(cr) as applicable.

fs DW: Un-factored stress at edge of flange for controlling steel flange due to vertical composite future wearing surface loads as calculated below (ksi).

MDW / Sc(3n) or MDW / Sc(cr) as applicable.

 $f_s$  (4+IM): Un-factored stress at edge of flange for controlling steel flange due to vertical composite live plus impact loads as calculated below (ksi).

M + IM / Sc(n) or M + IM / Sc(cr) as applicable.

fs (Service II): Sum of stresses as computed below (ksi). fsDC1 + fsDC2 + fsDW + 1.3 fs + im

0.95RhFyf: Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).

fs (Total)(Strength I): Sum of stresses as computed below on non-compact section (ksi).

1.25 (fsDC1 + fsDC2) + 1.5 fsDW + 1.75 fs \mathbb{1} + IM

Øf Fn: Non-Compact composite positive or negative stress capacity for Strength I loading according to Article 6.10.7 or 6.10.8 (ksi).

Vf: Maximum factored shear range in composite portion of span computed according to Article 6.10.10.

Descrip: LRFD data tables (Composite in negative moment regions)

INTER	IOR GIF	RDEF	R MC	MEN	IT :	ТΑ	BLE		
		0.4	Sp.	1 0	r 0	.6	5p.	2	Pier
İs	(in⁴)								
Ic(n)	(in³)								
Ic(3n)	(in³)								
Ic(cr)	(in <sup>a</sup> )								
55	(in³)								
Sc(n)	(in³)								
Sc(3n)	(in³)								
Sc(cr)	(in³)								
DC1	(k/')								
MDC1	('k)								
DC2	(k/')								
MDC2	('k)								
DW	(k/')								
MDW	('k)								
ME + IM	('k)								
Mu (Strength I)	('k)								
Øf Mn	('k)								
fs DC1	(ksi)								
fs DC2	(ksi)								
fs DW	(ksi)								
fs (4+IM)	(ksi)								
fs (Service II)	(ksi)								
0.95Rh Fyf	(ksi)								
fs (Total)(Strength									
Øf Fn	(ksi)								
Vf	(k)								

INTERIOR GIR	DER REACT	ON TABLE
	Abut.	Pier
RDC1 (k)		
RDC2 (k)		
RDW (k)		
R + IM (k)		
RTotal (k)		

Is, Ss: Non-composite moment of inertia and section modulus of the steel section used for computing fs(Total-Strength I, and Service II) due to non-composite dead loads (in.4 and in.3).

Ic(n), Sc(n): Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing fs(Total-Strength I, and Service II) in uncracked sections due to short-term composite live loads (in.4 and in.3).

Ic(3n), Sc(3n): Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing fs(Total-Strength I, and Service II) in uncracked sections, due to long-term composite (superimposed) dead loads (in: and in:3).

Ic(cr), Sc(cr): Composite moment of inertia and section modulus of the steel and longitudinal deck reinforcement, used for computing fs (Total-Strength 1 and Service II) in cracked sections, due to both short-term composite live loads and long-term composite (superimposed) dead loads (in.4 and in.3).

DC1:Un-factored non-composite dead load (kips/ft.).

MDC1: Un-factored moment due to non-composite dead load (kip-ft.).

DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

MDW: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).

Mk + IM: Un-factored live load moment plus dynamic load allowance (impact) (kip-ft.).

Mu (Strength I): Factored design moment (kip-ft.).

1.25 (MDC1 + MDC2) + 1.5 MDW + 1.75 ML + IM

Of Mn: Compact composite positive moment capacity computed according to Article 6.10.7.1 or non-slender negative moment capacity according to Article A6.1.1 or A6.1.2 (kip-ft).

fs DCI: Un-factored stress at edge of flange for controlling steel flange due to vertical non-composite dead loads as calculated below (ksj). MDC1/ Snc

fs DC2: Un-factored stress at edge of flange for controlling steel flange due to vertical composite dead loads as calculated below (ksjl.

MDC2/ Sc(3n) or MDC2/ Sc(cr) as applicable.

fs DW: Un-factored stress at edge of flange for controlling steel flange due to vertical composite future wearing surface loads as calculated below (ksi).

MDW/ Sc(3n) or MDW/ Sc(cr) as applicable.

fs (L+IM): Un-factored stress at edge of flange for controlling steel flange due to vertical composite live load plus impact loads as calculated below (ksi).

 $Mlambda+ {
m IM} \ / \ {
m Sc(n)} \ {
m or} \ {
m MDW} \ / \ {
m Sc(cr)} \ {
m as} \ {
m applicable}.$ 

fs (Service II): Sum of stresses as computed below (ksi). fsDC1 + fsDC2 + fsDW + 1.3 fs(+ + im)

0.95RhFyf: Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).

fs (Total)(Strength I): Sum of stresses as computed below on non-compact section (ksi).

1.25 (fsDC1 + fsDC2) + 1.5 fsDW + 1.75 fs(£ + IM)

Of Fn: Non-Compact composite positive or negative stress capacity for Strength I loading according to Article 6.10.7 or 6.10.8 (ksi). Vf: Maximum factored shear range in span computed according

to Article 6.10.10.

#### Note.

 $M_k$  and  $R_k$  include the effects of centrifugal force and superelevation.

Descrip: LRFD data tables for curved girders

INTERIO	OR GIF	RDER MOME	NT TABLE	
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	011	0.4 Sp. 1	Pier	0.6 Sp. 2
Is	(in⁴)			
Ic(n)	(in4)			
Ic(3n)	(in4)			
Ic(cr)	(in⁴)			
Ss	(in <sup>3</sup> )			
Sc(n)	(in³)			
Sc(3n)	(in3)			
Sc(cr)	(in³)			
Sxc	(in3)			
DC1	(k/')			
MDC1	('k)			
DC2	(k/')			
MDC2	('k)			
DW	(k/')			
MDW	('k)			
ME + IM	('k)			
fl (Strength I)	('k)			
Mu + ⅓fl Sxc	('k)			
Øf Mn	('k)			
fs DC1	(ksi)			
fs DC2	(ksi)			
fs DW	(ksi)			
fs (4+IM)	(ksi)			
fl (Service II)	(ksi)			
fs+ <sup>ft</sup> / <sub>2</sub> (Service II)	(ksi)			
0.95Rh Fyf	(ksi)			
$fs + f_{3}^{f}$ (Total)(Strength I)	(ksi)			
Øf Fn	(ksi)			
Vf	(k)			
	1/			

INTERIOR GIRDER REACTION TABLE								
		N. Abut.	Pier	S. Abut.				
RDC1	(k)							
RDC2	(k)							
RDW	(k)							
R £ + 111	(k)							
RTotal	(k)							

15, Ss: Non-composite moment of inertia and section modulus of the steel section used for computing fs[Total-Strength I, and Service II) due to non-composite dead loads (in.4 and in.3).

Ic(n), Sc(n): Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "m", used for computing fs(Total-Strength I, and Service II) in uncracked sections due to short term composite live loads (in.1 and in.1).

Ic(3n), Sc(3n): Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing fs(Total-Strength I, and Service II) in uncracked sections due to long-term composite (superimposed) dead loads (in.4 and in.3).

Ic(cr), Sc(cr): Composite moment of inertia and section modulus of the steel and longitudinal deck reinforcement, used for computing fs(Total-Strength 1 and Service 11) in cracked sections, due to both short-term composite live loads and long-term composite (superimposed) dead loads (in.4 and in.2).

Sxc: Section modulus about the major axis of section to the controlling flange, tension or compression, taken as yield moment with respect to the controlling flange over the yield strength of the controlling flange (in:).

DC1: Un-factored non-composite dead load (kips/ft.).

MDC1: Un-factored moment due to non-composite dead load (kip-ft.). DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

MDW: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).

Mt + IM: Un-factored live load moment plus dynamic load allowance (impactWkip-ft.).

Mu (Strength I): Factored design moment (kip-ft.).

1.25 (MDC1+ MDC2) + 1.5 MDW + 1.75 ML + IM

fl: Factored calculated normal stress at edge of flange for controlling flange plate due to lateral bending, Strength I or Service II as applicable (kip-ft.).

Of Mn: Compact composite positive moment capacity computed according to Article 6.10.7.1 or non-slender negative moment capacity according to Article A6.1.1 or A6.1.2 (kin-ft.)

fs DC1: Un-factored stress at edge of flange for controlling steel flange due to vertical non-composite dead loads as calculated below (ksi). MDC1 / Snc

fs DC2: Un-factored stress at edge of flange for controlling steel flange due to vertical composite dead loads as calculated below (ksi).

MDC2 / Sc(3n) or MDC2 / Sc(cr) as applicable.

MDC2 / Sc(3n) or MDC2 / Sc(cr) as applicable. fs DW: Un-factored stress at edge of flange for controlling steel

fision-factored stress at edge of flange for controlling stee flange due to vertical composite future wearing surface loads as calculated below (ksi).

MDW / Sc(3n) or MDW / Sc(cr) as applicable.

fs (L+IM): Un-factored stress at edge of flange for controlling steel flange due to vertical composite live plus impact loads as calculated below (ksi).

M½+ IM / Sc(n) or MDW / Sc(cr) as applicable

 $fs + fl/_2$  (Service II): Sum of stresses as computed below (ksi).  $fsDC1 + fsDC2 + fsDW + 1.3 fs(\{tr(M)\} + fl/_2)$ 

0.95RhFyf: Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).

 $fs + {}^{t}V_{3}$  (Total)(Strength I): Sum of stresses as computed below on non-compact section (ksi)

1.25 (fsDC1 + fsDC2) + 1.5 fsDW + 1.75 fs( $\frac{1}{2} + \frac{1}{100}$ ) +  $\frac{1}{1/3}$ Of Fn: Non-Compact composite positive or negative stress capacity for

Strength I loading according to Article 6.10.7 or 6.10.8 (ksi). Vf: Maximum factored shear range in span computed according to Article 6.10.10.

 $M_{\Sigma}$  and  $R_{\Sigma}$  include the effects of centrifugal force and superelevation.

Descrip: LRFD PPC I beam data tables

INTERIOR BEAM MOMENT TABLE								
		0.4 Sp. 1 0.6 Sp. 3	Pier 1 or 2	0.5 Sp. 2				
I	(in⁴)							
I'	(in⁴)							
Sb	(in³)							
Sb'	(in³)							
St	(in³)							
St'	(in³)							
DC1	(k/')							
MDC1	('k)							
DC2	(k/')							
MDC2	('k)							
DW	(k/')							
MDW	('k)	-						
MŁ + IM	('k)							

	INTERIOR BEAM REACTION TABLE									
		Abut.	Pier Pier	1 2	Span Span	1 3	Pier Pier	1 2	Span Span	2 2
	RDC1 (k)									
*	RDC2 (k)									
*	RDW (k)									
*	R + IM (k)									
	RTotal (k)	·								

<sup>\*</sup> At continuous piers, reactions from composite loads are assumed to be equally distributed to each bearing line.

- I: Non-composite moment of inertia of beam section (in.4).
- I': Composite moment of inertia of beam section (in.4).
- Sb: Non-composite section modulus for the bottom fiber of the prestressed beam (in.<sup>3</sup>).
- Sb': Composite section modulus for the bottom fiber of the prestressed beam  $(in.^3)$ .
- St: Non-composite section modulus for the top fiber of the prestressed beam (in.3).
- St: Composite section modulus for the top fiber of the prestressed beam (in.3).
- DC1: Un-factored non-composite dead load (kips/ft.).
- MDC1: Un-factored moment due to non-composite dead load (kip-ft.).
- DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).
- MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).
  - DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).
- MDW: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft).
- M½ + IM: Un-factored live load moment plus dynamic load allowance (impact) (kip-ft.).

Descrip: LFD data tables

	IN	ITERIOR GIF	RDER M	OMENT	TAB.	LE		
			0.4 Sp.	1 or	0.6 5	p. 2	Pier	
	Is	(in⁴)						
	Ic(n)	(in⁴)						
	Ic(3n)	(in⁴)						
	Ss	(in³)						
	Sc(n)	(in³)						
	Sc(3n)	(in³)						
	Z	(in³)						
	₽	(k/')						
	MР	('k)						
	s P	(k/')						
	МsР	('k)						
	ΜŁ	('k)						
	MIM	('k)						
	<sup>5</sup> 3 [M½ + 1]	('k)						
	Ма	('k)						
*	Ми	('k)						
	fs⊉non-comp	(ksi)						
	fs₽ (comp)	(ksi)						
	fs <sup>5</sup> 3 [M Ł + M <sub>I</sub>							
	fs (Overload)	(ksi)						
**	fs (Total)	(ksi)						
	VR	(k)						

INTE	INTERIOR GIRDER REACTION TABLE							
		Pier						
R₽	(k)							
R Ł	(k)							
Rı	(k)							
RTotal	(k)							

<sup>\*</sup> Compact section

- Is, Ss: Non-composite moment of inertia and section modulus of the steel section used for computing fs(Total and Overload) due to non-composite dead loads (in.4 and in.3).
- Ic(n), Sc(n): Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing fs(Total and Overload) due to short-term composite live loads (in.4 and in.3).
- Ic(3n), Sc(3n): Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing fs(Total and Overload) due to long-term composite (superimposed) dead loads (in.4 and in.3).
  - Z: Plastic Section Modulus of the steel section in non-composite areas (in.3).
  - P: Un-factored non-composite dead load (kips/ft.).
  - MP: Un-factored moment due to non-composite dead load (kip-ft.).
  - s ?: Un-factored long-term composite (superimposed) dead load (kins/ft.)
  - $M_s \mathbb{Q}$ : Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).
  - Mt: Un-factored live load moment (kip-ft.).
  - MI: Un-factored moment due to impact (kip-ft.).
  - Ma: Factored design moment (kip-ft.). 1.3 [M $^{\circ}$  + Ms $^{\circ}$  +  $\frac{5}{3}$  (M $^{\circ}$  + MI)]
  - Mu: Compact composite moment capacity according to AASHTO LFD 10.50.1.1 or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).
- fs (Overload): Sum of stresses as computed from the moments below (ksi).  $MP + MsP + \frac{5}{3} (M! + MI)$ 
  - fs (Total): Sum of stresses as computed from the moments below on non-compact section (ksi).  $1.3 \ [\text{MP} + \text{MsP} + \frac{5}{3} \ (\text{ML} + \text{MI})]$ 
    - VR: Maximum\(\psi\) + impact shear range within the composite portion of the span for stud shear connector design (kips).

<sup>\*\*</sup> Braced non-compact and partially braced section

Descrip: LFD data tables for curved girders

INTERIOR GIRDER MOMENT TABLE								
		0.4 Sp. 1	Pier	0.6 Sp. 2				
Is	(in⁴)							
Ic(n)	(in⁴)							
Ic(3n)	(in⁴)							
Ss	(in³)							
Sc(n)	(in³)							
Sc(3n)	(in³)							
Sl	(in³)							
P	(k/')							
M₽	('k)							
5₽	(k/')							
Ms ₽	('k)							
M Ł	('k)							
MI	('k)							
<sup>5</sup> 3[M½ + MI]	('k)							
Ма	('k)							
Mbl	('k)							
fsℚ(non-comp)	(ksi)							
fs₽(comp)	(ksi)							
fs <sup>5</sup> 3 [M½+ M <sub>I</sub> ]	(ksi)							
fl	(ksi)							
fs(Overload)	(ksi)							
fs(Total)	(ksi)							
Fcr(Overload)	(ksi)							
VR	(k)							
Fcr	(ksi)							

INTERIOR GIRDER REACTION TABLE							
		N. Abut.	Pier	S. Abut.			
R₽	(k)						
R4	(k)						
RI	(k)						
RTotal	(k)						

- Is, Ss: Non-composite moment of inertia and section modulus of the steel section used for computing fs(Total and Overload) due to non-composite dead loads (in.4 and in.3).
- Ic(n), Sc(n): Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing fs(Total and Overload) due to short-term composite live loads (in.4 and in.3).
- Ic(3n), Sc(3n): Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing fs(Total and Overload) due to long-term composite (superimposed) dead loads (in.4 and in.3).
  - Sl: Section modulus of one flange plate for lateral flange bending (in.3).
  - p: Un-factored non-composite dead load (kips/ft.).
  - $M\overline{\mathbb{P}}$ : Un-factored moment due to non-composite dead load (kip-ft).
  - sp: Un-factored long-term composite (superimposed) dead load (kips/ft.).
  - Ms@: Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).
  - M\(\frac{1}{2}\): Un-factored live load moment (kip-ft.).
  - MI: Un-factored moment due to impact (kip-ft).
  - Ma: Factored design moment (kip-ft.). 1.3 [M $^{\circ}$  + Ms $^{\circ}$  +  $\frac{5}{3}$  (M $^{\circ}$  + MI)]
  - Mbl: Factored lateral bending moment for flange plate (kip-ft.).
  - fl: Factored calculated normal stress at the edge of flange due to lateral bending (ksi).
- fs(Overload): Sum of stresses as computed from the moments below (ksi).  $MP + MSP + \frac{5}{2}(M! + MI)$ 
  - fs(Total): Sum of stresses as computed from the moments below (ksi). 1.3  $[MP + MsP + \frac{5}{2}(M! + MI)]$
- Fcr(Overload): Critical average flange stress at overload computed according to the 2003 AASHTO Guide Specifications for Horizontally Curved Steel Girder Highway Bridges Section 9.5 (ksi.).
  - Fcr: Critical average flange stress (smaller of Fcr1 or Fcr2 for partially braced flanges and F for continuously braced flanges) computed according to the 2003 AASHTO Guide Specifications for Horizontally Curved Steel Girder Highway Bridges (Sections 5.2, 5.3 and 5.4) (ksi).
  - VR: Maximum\(\frac{1}{2} + impact shear range within span for stud shear connector design (kips).

#### Note:

 $M \not$  and  $R \not$  include the effects of centrifugal force and superelevation.

Descrip: LFD PPC I beam data tables

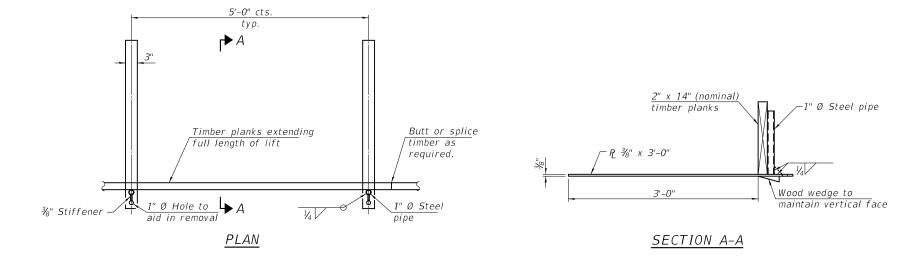
INTERIOR BEAM MOMENT TABLE					
		0.4 Sp. 1 0.6 Sp. 3	Pier 1 or 2	0.5 Sp. 2	
I	(in⁴)				
I'	(in⁴)				
Sb	(in³)				
Sb'	(in³)				
St	(in³)				
St'	(in³)				
P	(k/')				
MР	('k)				
5 P	(k/')				
MsP	('k)				
M Ł	('k)				
MI	('k)				

- 1	INTERIOR BEAM REACTION TABLE										
			Abut.	Pier	1	Span	1	Pier	1	Span	2
			Abut.	Pier	2	Span	3	Pier	2	Span	2
	R ₽ (k.	)									
*	$R_s Q$ (k)	)									
*	R ½ (k.	)									
*	RI (k	)									
	RTotal (k	) [									

<sup>\*</sup> At continuous piers, reactions from composite loads are assumed to be equally distributed to each bearing line.

- I: Non-composite moment of inertia of beam section (in.4).
- I': Composite moment of inertia of beam section (in.4).
- Sb: Non-composite section modulus for the bottom fiber of the prestressed beam (in.3).
- Sb': Composite section modulus for the bottom fiber of the prestressed beam (in.3).
- St: Non-composite section modulus for the top fiber of the prestressed beam (in.3).
- St': Composite section modulus for the top fiber of the prestressed beam (in.3).
- ₽: Un-factored non-composite dead load (kips/ft.).
- MP: Un-factored moment due to non-composite dead load conservatively taken at 0.5 of the span (kip-ft.).
- sp: Un-factored long-term composite (superimposed) dead load (kips/ft.).
- MsQ: Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).
- M½: Un-factored live load moment on the composite section (kip-ft.).
- MI: Un-factored moment due to impact on the composite section (kip-ft.).

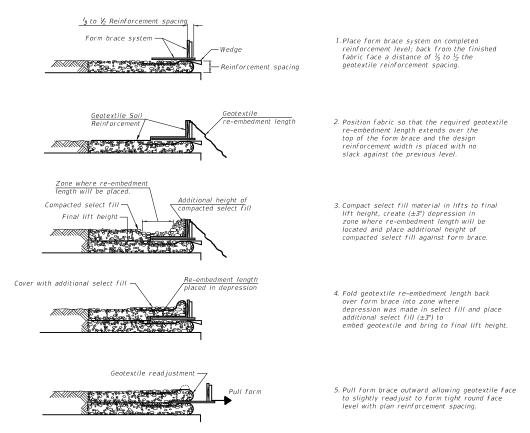
Descrip: Geotextile wall form brace details



<u>GEOTEXTILE</u> <u>FORM BRACE DETAIL</u> Note:

This is a suggested detail, the Contractor is responsible for the design of the form brace system to be used.

Descrip: Geotextile wall procedure

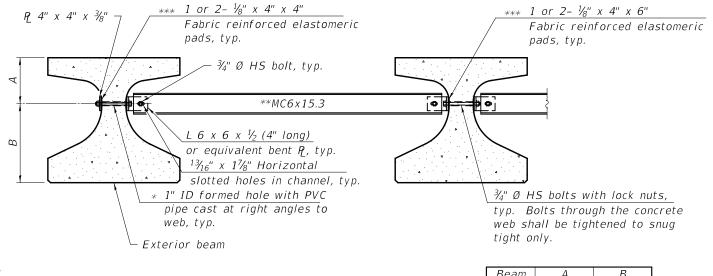


#### <u>GEOTEXTILE WALL</u> <u>CONSTRUCTION SEQUENCE</u>

#### Note

The geotextile soil reinforcement shall have a minimum allowable tensile strength (T min.) of lb./in. as determined by the procedure described in the Special Provision. The computations supporting the determination of (T min.) shall be submitted to the engineer for approval.

Descrip: Permanent bracing details for IL27 & IL36 beams



#### Notes:

All material for bracing shall be hot dip galvanized according to AASHTO M111 unless otherwise noted.

Two hardened washers are required for each set of oversized holes.

All holes shall be  $^{15}\!\!/_{16}$ " Ø unless otherwise noted.

 $\frac{5}{16}$ " x 3" x 3" plate washers are required over all slotted holes.

All bolts shall be galvanized according to AASHTO M232. Bracing shall be installed as beams are erected and

tightened as soon as possible during erection.

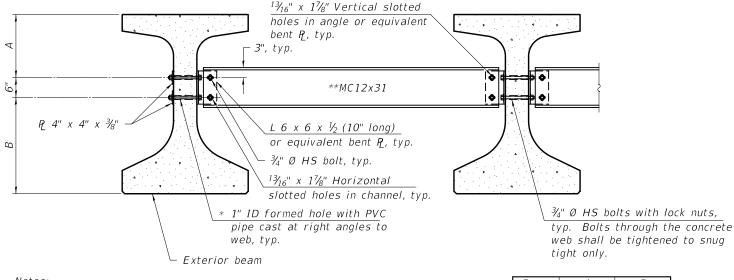
Permanent bracing shall not be paid for separately, but shall be included in the cost of Furnishing and Erecting Precast Prestressed Concrete Beams.

D C Giiii	/ '	-
IL27	1111/4"	1'-3¾"
IL36	1'-11/4"	1'-10¾"

- \* Fabricator shall locate to miss strands within permissible tolerances.
- \*\* Alternate MC6x18 channels are permitted to facilitate material acquisition.
- \*\*\* Place pads as necessary to provide a flat mounting surface between the steel and concrete.

PERMANENT BRACING DETAILS FOR
IL27 AND IL36 BEAMS

Descrip: Permanent bracing details for IL45 & IL54 beams



Notes:

All material for bracing shall be hot dip galvanized according to AASHTO M111 unless otherwise noted.
Two hardened washers are required for each set of

Two hardened washers are required for each set oversized holes.

All holes shall be  $^{15}\!\!/_{16}$ " Ø unless otherwise noted.  $^{5}\!\!/_{16}$ " x 3" x 3" plate washers are required over all slotted holes.

All bolts shall be galvanized according to AASHTO M232. Bracing shall be installed as beams are erected and tightened as soon as possible during erection.

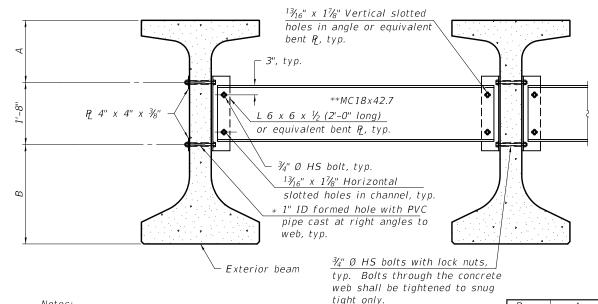
Permanent bracing shall not be paid for separately, but shall be included in the cost of Furnishing and Erecting Precast Prestressed Concrete Beams.

Beam	Α	В
IL45	1'-3"	2'-0"
IL54	1'-7"	2'-5"

- \* Fabricator shall locate to miss strands within permissible tolerances.
- \*\* Alternate MC12x35 channels are permitted to facilitate material acquisition.

PERMANENT BRACING DETAILS FOR
IL45 AND IL54 BEAMS

Descrip: Permanent bracing details for IL63 & IL72 beams



#### Notes:

All material for bracing shall be hot dip galvanized according to AASHTO M111 unless otherwise noted.

Two hardened washers are required for each set of oversized holes.

All holes shall be  $^{15}\!\!/_{16}$ " Ø unless otherwise noted.  $\frac{5}{16}$ " x 3" x 3" plate washers are required over all slotted holes.

All bolts shall be galvanized according to AASHTO M232. Bracing shall be installed as beams are erected and tightened as soon as possible during erection.

Permanent bracing shall not be paid for separately, but shall be included in the cost of Furnishing and Erecting Precast Prestressed Concrete Beams.

\* Fabricator shall locate to miss strands within permissible tolerances.

1'-4"

1'-8"

Beam

IL63

*IL72* 

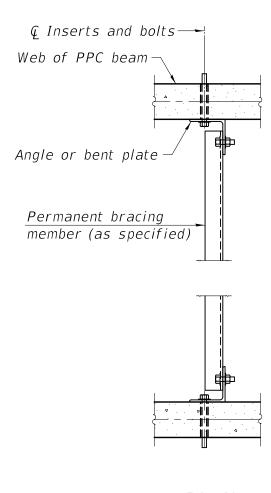
\*\* Alternate MC18x45.8 channels are permitted to facilitate material acquisition.

2'-3"

2'-8"

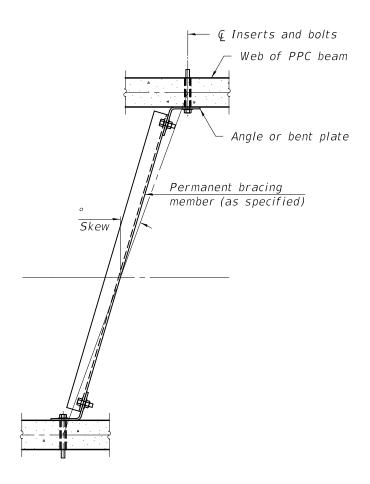
PERMANENT BRACING DETAILS FOR IL63 AND IL72 BEAMS

Descrip: Permanent bracing detail - No skew



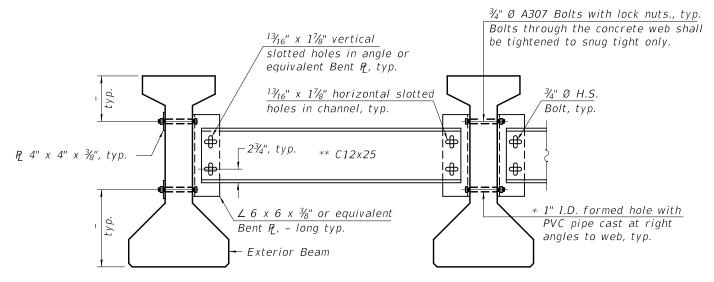
<u>PLAN</u> (When 90° bracing is specified)

Descrip: Permanent bracing detail - Skewed



<u>PLAN</u> (When skewed bracing is specified)

Descrip: Permanent bracing details for 36" & 42" PPC I beams



#### Notes:

All material for bracing shall be hot dip galvanized according to AASHTO M111 unless otherwise noted.

Two hardened washers are required for each set of oversized holes.

All holes shall be  $^{15}\!\!/_{16}$ " Ø unless otherwise noted.  $^{5}\!\!/_{16}$ " x 3" x 3" plate washers are required over all slotted holes.

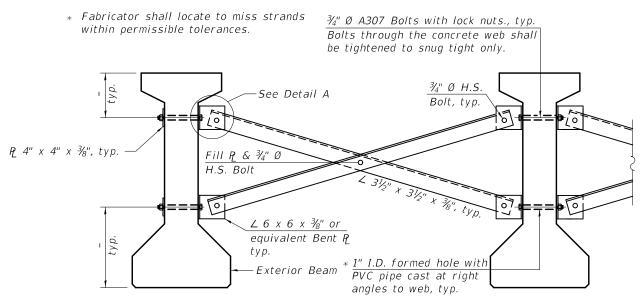
All bolts shall be galvanized according to AASHTO M232. Bracing shall be installed as beams are erected and tightened as soon as possible during erection.

Permanent bracing shall not be paid for separately, but shall be included in the cost of Furnishing and Erecting Precast Prestressed Concrete I-Beams.

- Fabricator shall locate to miss strands \* within permissible tolerances.
- \*\* Alternate C12x30 channels are permitted to facilitate material acquisition.

PERMANENT BRACING DETAILS FOR 36" AND 42" PPC I-BEAMS

Descrip: Permanent bracing details for 48" & 54" PPC I beams



#### Notes:

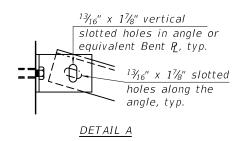
All material for bracing shall be hot dip galvanized according to AASHTO M111 unless otherwise noted.

Two hardened washers are required for each set of oversized holes.

All holes shall be  $^{15}\!\!/_{16}$ " Ø unless otherwise noted.  $^{5}\!\!/_{16}$ " x 3" x 3" plate washers are required over all slotted holes.

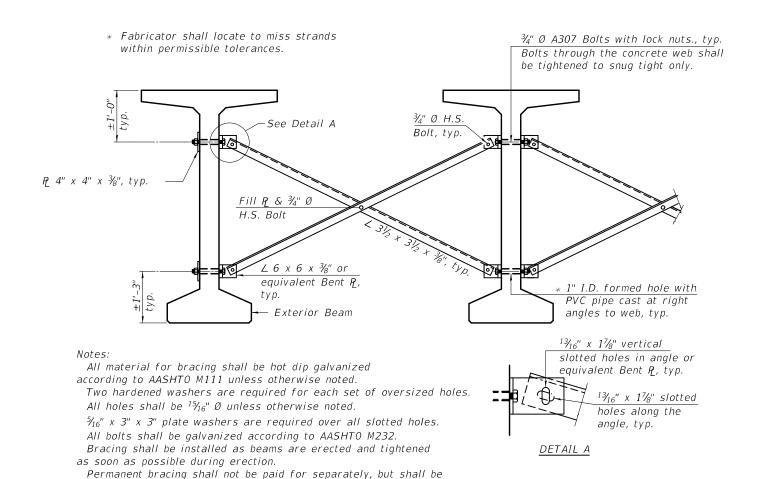
All bolts shall be galvanized according to AASHTO M232. Bracing shall be installed as beams are erected and tightened as soon as possible during erection.

Permanent bracing shall not be paid for separately, but shall be included in the cost of Furnishing and Erecting Precast Prestressed Concrete I-Beams.



PERMANENT BRACING DETAILS FOR 48" AND 54" PPC I-BEAMS

Descrip: Permanent bracing details for Bulb T beams



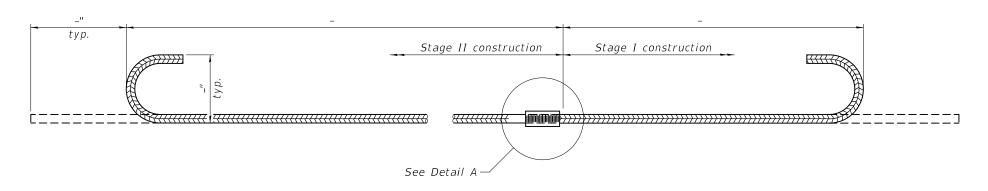
PERMANENT BRACING DETAILS
FOR BULB-T BEAMS

included in the cost of Furnishing and Erecting Precast Prestressed

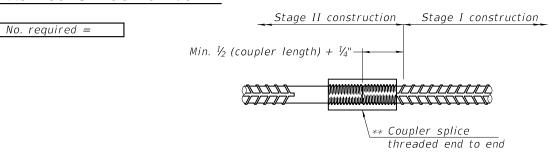
Concrete Bulb T-Beams.

Descrip: Bar splicer assembly for edge beams at stage construction joint

\*\* The bar splicer assembly shall allow completion of the splice without turning of the hook bars. The stage II splice bar shall be threaded such that the entire coupler can be threaded onto the splice bar.

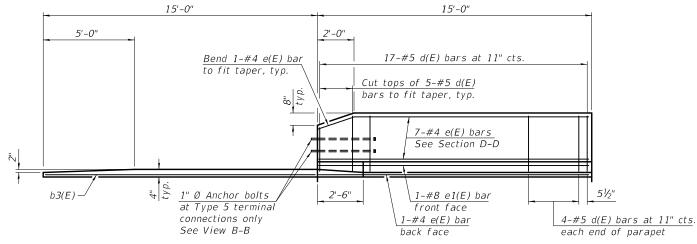


## #- a-(E) BAR SPLICER ASSEMBLY FOR EDGE BEAMS AT STAGE CONSTRUCTION JOINT



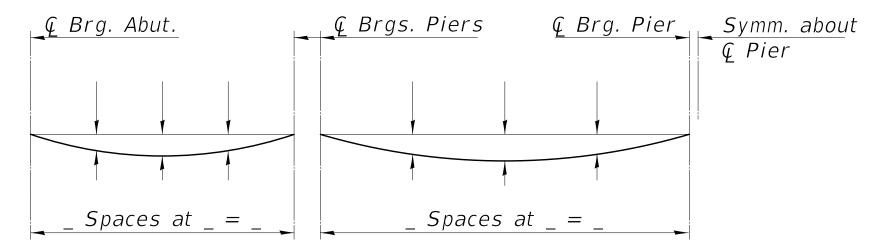
DETAIL A

Descrip: View E-E for Bridge approach slabs with 42" parapets



VIEW E-E

Descrip: Dead load deflection diagram for top of slab elevations



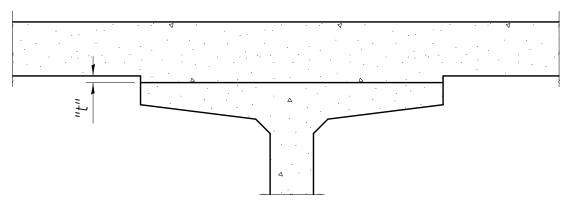
## DEAD LOAD DEFLECTION DIAGRAM

(Includes weight of concrete, excluding beams).

### Note:

The above deflections are not to be used in the field if the engineer is working from the grade elevations adjusted for dead load deflections as shown below.

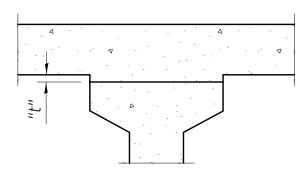
Descrip: PPC Bulb T-beam fillet height detail for top of slab elevations



To determine "t": After all precast prestressed beams have been erected, elevations of the top flanges of the beams shall be taken at intervals shown below. These elevations subtracted from the "Theoretical Grade Elevations Adjusted for Dead Load Deflections" shown below, minus slab thickness, equals the fillet heights "t" above top flanges of beams.

## FILLET HEIGHTS

Descrip: PPC I-beam fillet height detail for top of slab elevations



To determine "t": After all precast prestressed beams have been erected, elevations of the top flanges of the beams shall be taken at intervals shown below. These elevations subtracted from the "Theoretical Grade Elevations Adjusted for Dead Load Deflections" shown below, minus slab thickness, equals the fillet heights "t" above top flanges of beams.

## FILLET HEIGHTS